

Linear Edge Stability and Toroidal Rotation



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Introduction



MHD model for ELMs:

- ELMs are MHD instabilities localized near the plasma edge
- low-n (toroidal mode number) peeling modes driven by edge current (bootstrap current), highly localized
- high-n ballooning modes driven by edge pressure gradient, more extended
- intermediate-n coupled peeling-ballooning modes (e.g. Snyder et al., PPCF 46; 2004)

Effects of Sheared Toroidal Rotation:

- analytical theory (e.g. Connor et al., PPCF **46**, 2004; Furukawa et al., PPCF **46**, 2004) predicts stabilization of high-n ballooning modes in the s- α -model
- limitations: high n, large aspect ratio, no shaping
- 'Doppler shift': linear growth rate $\gamma \to \gamma + in \Omega(r)$ where $\Omega(r)$ is the rotation frequency
- discontinuity in the linear growth rate $\gamma(\Omega)$ for $n\to\infty$
- linear stability limits, most unstable mode number, mode extend and mode phase



Linear MHD Stability Analysis



normalized MHD equations:

• continuity equation

$$\frac{\partial \rho}{\partial t} = -\nabla \cdot (\rho \mathbf{v})$$

• momentum equation

$$\rho \frac{\mathrm{d}\mathbf{v}}{\mathrm{d}t} = -\nabla p + (\nabla \times \mathbf{B}) \times \mathbf{B}$$

• induction equation $\frac{\partial \mathbf{B}}{\partial t} = \nabla \times (\mathbf{v} \times \mathbf{B}) - \nabla \times (\eta \nabla \times \mathbf{B})$

• energy equation

$$\frac{\partial T}{\partial t} = -\mathbf{v} \cdot \nabla T - (\gamma - 1) T \nabla \cdot \mathbf{v}$$

 \bullet divergence of ${\bf B}$

$$\nabla \cdot \mathbf{B} = 0$$

linear MHD stability codes:

- CASTOR_FLOW: compressible, resistive, toroidal rotation, full set of equations, normal mode analysis (Huysmans 1991, Kerner el al. 1998, Strumberger 2005)
- MISHKA: incompressible, ideal, diamagnetic effects, reduced set of equations, normal mode analysis (Huysmans et al., Phys. Plasmas 8; 2001)
- ELITE: compressible, ideal, toroidal rotation, solves Euler equations derived from perturbed energy δW -ansatz (Wilson et al., Phys. Plasmas; 2002)



Toroidal Rotation



Aim: Study the influence of sheared toroidal rotation of the form

 ${f V_0}=R^2\Omega_0(s)\,
abla\phi\,$, i.e. contravariant component $\,V_0^3=\Omega_0(s)\,$

on the linear stability of the plasma edge for subsonic toroidal rotation velocities.

<u>available tools:</u>

- CASTOR_FLOW: toroidal and poloidal rotation; for low to intermediate toroidal mode numbers ($n \le 25$) or simple equilibria (E. Strumberger)
- ELITE: toroidal rotation; for intermediate to high toroidal mode numbers $(n \ge 8)$ (P.B. Snyder)
- MISHKA_FLOW: toroidal rotation; for low to intermediate toroidal mode numbers (I. Chapman,S. Saarelma)





Linearization of MHD equations with perturbation ansatzplasma variables $F = F_0 + \tilde{F}$ equilibrium part F_0 perturbed part $\tilde{F} = \sum c_{n,m} \exp(im\theta) \times \exp(in\phi) \exp(\lambda t)$

 $\begin{array}{l} \mbox{complex eigenvalue } \lambda = \gamma + i \omega \\ \mbox{with growth rate } \gamma \mbox{ and mode frequency } \omega \end{array}$

no linear coupling of toroidal modes \boldsymbol{n} because of axisymmetry







- normal mode analysis
- solves large matrix equation iteratively
- full MHD system with 8 plasma variables ($\tilde{\rho}$, \tilde{T} , $\tilde{\mathbf{v}}$, $\tilde{\mathbf{B}}$), or reduced MHD system with 7 plasma variables ($\tilde{\rho}$, $\tilde{\mathbf{v}}$, $\tilde{\mathbf{B}}$)
- toroidal mode numbers on 4GB machine:
 - $n \lesssim 10$ for experimental equilibria and high edge q,
 - $n \lesssim 60$ for moderate q analytical equilibria

full MHD system: (Strumberger et al. NF 45, 2005)

• continuity equation

$$\lambda \tilde{\rho} = -\rho_0 \nabla \cdot \tilde{\mathbf{v}} - \tilde{\mathbf{v}} \cdot \nabla \rho_0 - \mathbf{v_0} \cdot \nabla \tilde{\rho}$$

• temperature equation

$$\lambda \tilde{T} = -\tilde{\mathbf{v}} \cdot \nabla T_0 - \mathbf{v_0} \cdot \nabla \tilde{T} - (\Gamma - 1) T_0 \nabla \cdot \tilde{\mathbf{v}}$$



CASTOR_FLOW (continued)



• momentum equation $\lambda \rho_0 \tilde{\mathbf{v}} = -\tilde{\rho} (\mathbf{v_0} \cdot \nabla) \mathbf{v_0} - \rho_0 (\tilde{\mathbf{v}} \cdot \nabla) \mathbf{v_0} - \rho_0 (\mathbf{v_0} \cdot \nabla) \tilde{\mathbf{v}} - \nabla (\rho_0 \tilde{T})$ $-\nabla (\tilde{\rho} T_0) - \nabla \cdot \tilde{\Pi} + (\nabla \times \mathbf{B_0}) \times \tilde{\mathbf{B}} + (\nabla \times \tilde{\mathbf{B}}) \times \mathbf{B_0}$

• Ohm's law

$$\lambda \tilde{\mathbf{B}} = \nabla \times \left(\mathbf{v_0} \times \tilde{\mathbf{B}} + \tilde{\mathbf{v}} \times \mathbf{B_0} - \eta_0 \nabla \times \tilde{\mathbf{B}} \right)$$

with perturbed viscous force for ion Landau damping

$$-\left(\nabla \cdot \tilde{\Pi}\right)_{m} = -\kappa_{\parallel} |k_{\parallel} v_{\text{thi}} |\rho_{0} (v_{\parallel})_{m}$$

where $k_{\parallel}=\!\left(n-m/q\right)/R$ is the wave vector and $\kappa_{\parallel}\approx\sqrt{\pi}$





reduced MHD system:

neglect perturbed centrifugal force $-\tilde{\rho}(\mathbf{v_0} \cdot \nabla) \mathbf{v_0}$ in momentum equation replace continuity and temperature equation by

• pressure equation

$$\lambda \tilde{p} = -\tilde{\mathbf{v}} \cdot \nabla p_0 - \mathbf{v_0} \cdot \nabla \tilde{p} - \Gamma p_0 \nabla \cdot \tilde{v}$$

and

• reduced momentum equation

$$\begin{aligned} \lambda \rho_0 \tilde{\mathbf{v}} &= -\rho_0 (\tilde{\mathbf{v}} \cdot \nabla) \, \mathbf{v_0} - \rho_0 (\mathbf{v_0} \cdot \nabla) \, \tilde{\mathbf{v}} - \nabla \cdot \tilde{\Pi} \\ &+ (\nabla \times \mathbf{B_0}) \times \tilde{\mathbf{B}} + \left(\nabla \times \tilde{\mathbf{B}} \right) \times \mathbf{B_0} \end{aligned}$$

memory requirements and CPU time scale with square of number of variables





- normal mode analysis
- solves Euler equations derived from $\delta W\mbox{-ansatz}$ by shooting method
- force balance equation for the plasma displacement ξ with expansion in 1/n, keeping terms up to second order
- intermediate to high toroidal mode numbers $n\gtrsim 8$
- uses poloidal harmonic localization for efficiency

MHD system in terms of ξ :

$$\begin{split} &\Gamma \tilde{\rho} &= -\gamma \left[\left(\xi \cdot \nabla \right) \rho_0 + \rho_0 (\nabla \cdot \xi) \right] \\ &\Gamma \tilde{p} &= -\gamma \left[\left(\xi \cdot \nabla \right) p_0 + g p_0 (\nabla \cdot \xi) \right] \\ &\Gamma \tilde{\mathbf{B}} &= \gamma \nabla \times (\xi \times \mathbf{B}_0) + \frac{\gamma R^2 \Omega'}{\Gamma} \left[\left[\nabla \times (\xi \times \mathbf{B}_0) \right] \cdot \nabla \psi \right] \nabla \phi \end{split}$$

with Doppler shifted growth rate $\Gamma=\gamma+in\Omega$, ratio of specific heats g and $\Omega'=\mathrm{d}\Omega/\mathrm{d}\psi$



MISHKA_FLOW



- normal mode analysis
- based on reduced linear MHD eigenmode code MISHKA_D
- reduced MHD system with 7 plasma variables (\tilde{p} , $\tilde{\mathbf{v}}$, $\tilde{\mathbf{B}}$)
- intermediate toroidal mode numbers $n \lesssim 40$ for moderate to high q values
- includes diamagnetic drift terms (Huysmans et al. PoP 8(10), 2001)
- code recently developed by Ian Chapman (UKAEA Culham)



Benchmarks

IPP

Aims:

- study influence of sheared toroidal rotation on stability limits
- use CASTOR_FLOW for low to intermediate mode numbers and ELITE for high mode numbers
- compare stabilization by sheared toroidal rotation to stabilization by diamagnetic drifts (MISHKA_D)



benchmark CASTOR_FLOW vs. ELITE for an ideal plasma case (no rotation)



Circular Equilibrium cbm1_hel









<u>cbm1_hel:</u>

- ballooning unstable circular equilibrium
- well resolved
- low edge-q ≈ 2
- no shaping
- => weak poloidal coupling
- benchmark possible up to high toroidal mode numbers $n\sim 40$



Shear Profiles





rotation profile $\Omega(s) = \Omega_0(1 - s^{\chi})$ with $s = \sqrt{\psi/\psi_{\rm bd}}$ and $\chi = 2, \, 6, \, 10$



Benchmark: cbm1_hel





- excellent agreement of CASTOR_FLOW and ELITE for growth rates
- except for n = 50 (only 31 poloidal modes in CASTOR_FLOW)
- mode frequencies agree very well for n=8
- but constant factors for n = 20, 35, 50 (normalization issues?)



Benchmark: cbm1_hel (continued)













Benchmark cbm1_hel (continued)









MISHKA_FLOW:

- excellent agreement for n=8
- good agreement for n = 20 with CASTOR_FLOW mode frequencies
- \bullet good agreement for n=35 with ELITE mode frequencies
- possible problem with CASTOR_FLOW wave frequencies for high n but very good agreement for growth rates



Circular Equilibrium 'internal kink'







internal n = 1 kink:

- circular Bussac equilibrium
- unstable to n = 1 internal kink
- fixed boundary (no vacuum)
- $\bullet\,$ no shaping, low edge-q ≈ 2.5
- => weak poloidal coupling



Benchmark: 'internal kink'







• rigid rotation (no shear)

- excellent agreement in growth rates and mode frequencies between MISHKA_FLOW and CASTOR_FLOW
- $\bullet\,$ strong stabilization of the internal $n=1\,$ kink
- completely stabilized in MISHKA_FLOW, but finite growth rate in CASTOR_FLOW
- possibly due to missing viscous damping (to be tested), sound waves?, or destabilizing effect of centrifugal force



Toroidal Rotation: First Results







Results:

- stronger effects on high-n modes
- low shear generally destabilizing (centrifugal force)
- intermediate shear generally stabilizing
- high shear again destabilizing (Kelvin-Helmholtz?)
- localization of shear and affected mode region also matter





Mode Structures





Changes in Mode Structure:

- strongly destabilized mode n = 8 at very high shear and high rotation frequency
- no major change in mode structure
- internal modes slightly weakened
- entire mode shifted radially outward (centrifugal force)
- wide mode structure less affected by shear



Mode Structures (continued)





Changes in Mode Structure:

- weakly stabilized mode n = 35 at intermediate shear and high rotation frequency
- mode structure is smeared out and broadened
- internal modes strongly reduced
- mode center shifted radially inward (shear larger at edge)
- narrow edge mode strongly affected by shear



Mode Structures (continued)





Changes in Mode Structure:

- nearly unaffected mode n = 35 at very high shear and high rotation frequency
- mode structure broadened
- internal modes strongly reduced
- mode center shifted radially outward (centrifugal force reaches farther out)
- narrow edge mode strongly affected by shear
- compensation of destabilizing and stabilizing effects



Stabilization through Toroidal Rotation



stabilization of ballooning modes through rotational shear for a circular equilibrium (P. Snyder, 2005)

Toroidal Mode Number (n)

Toroidal Rotation with ELITE (P. Snyder):

- circular equilibrium, ballooning unstable
- stabilization for high toroidal mode numbers or high rotational shear
- destabilizing for low toroidal mode numbers and low shear



High Rotational Mach Numbers



Strumberger et al. NF 45, 2005

from force balance equation follows:

pressure
$$p(\psi, \theta) = \bar{p}(\psi) \exp\left(\frac{\Omega^2 R^2}{2c_{\rm s}^2}\right)$$

with sound speed $c_{\rm s} = \sqrt{k_{\rm B}T/m_{\rm i}}$

=> for high Mach numbers $M = \Omega R/c_{\rm s} \gtrsim 0.3$: pressure and density are not flux surface quantities anymore!

equilibrium code DIVA allows to calculate two-dimensional equilibria

CASTOR_FLOW allows stability analysis for equilibria with poloidally varying pressure and density



Summary and Outlook



Results:

- centrifugal force can be destabilizing for high rotation frequencies
- intermediate shear acts stabilizing on narrow modes
- strong shear can act destabilizing (Kelvin-Helmholtz)
- mode localization with respect to shear layer and mode extent important
- more detailed studies necessary to investigate effects of toroidal rotation

Linear Edge Stability and Toroidal Rotation:

- successful benchmark of CASTOR_FLOW, ELITE, and MISHKA_FLOW for circular equilibria with internal and edge localized modes
- next step: experimental equilibria (high-q, shaped)
- low-n mode studies with CASTOR_FLOW plus high-n mode studies with ELITE
- comparison of diagmagnetic drifts to toroidal rotation
- access to second stability regime by rotation effects?