

# Impurity radiation to control pedestal temperature: how to meet the constraints for an integrated scenario?

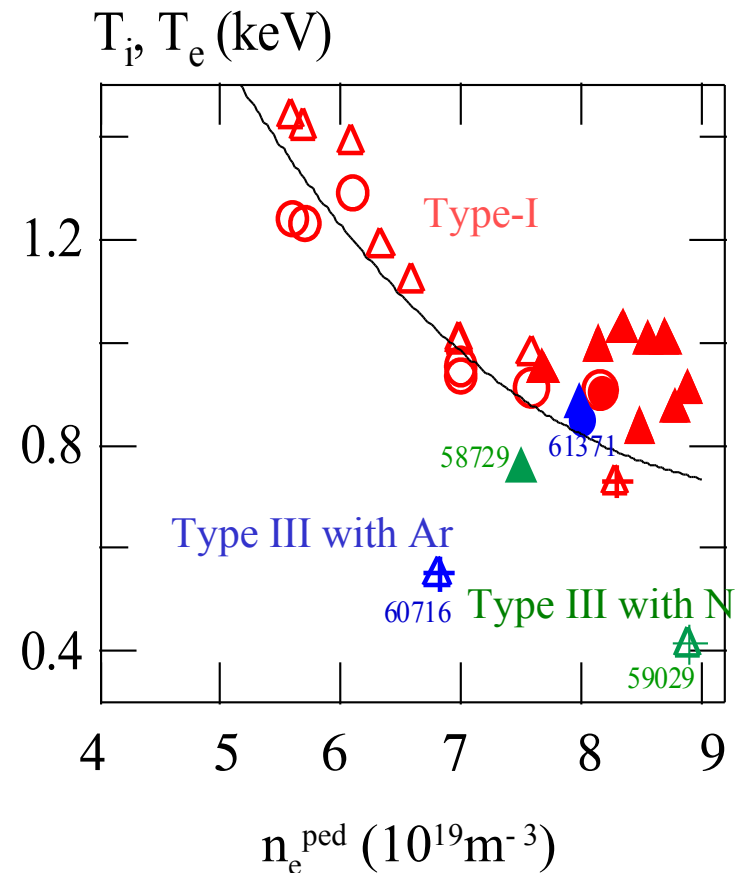
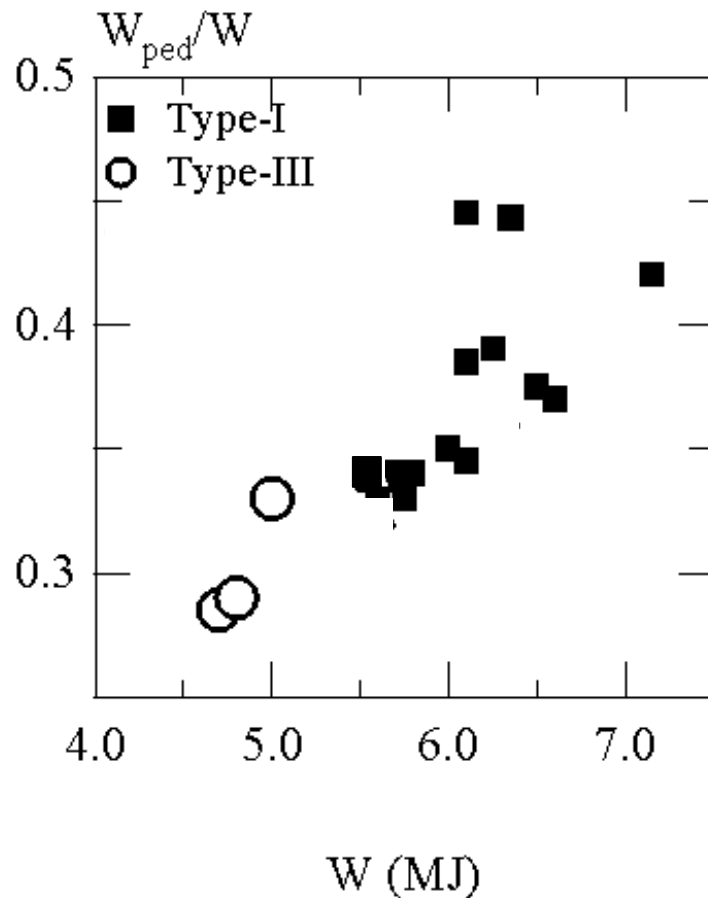
Presented by P. Monier-Garbet,

Thanks to all the contributors to this work

2. Introduction: what are the requirements?
2. Control of the pedestal temperature with impurity radiation?
3. Conclusion: integration?

In standard H-mode, high energy content requires:

- high  $W_{ped}$ : decreasing  $W_{ped} =$  decreasing  $W$  (profile stiffness)
- $P$  close to Type-I FI M value



## ELM control is needed. How?

1) confinement marginally affected: maintain  $\nabla P$  ~ at ballooning threshold

### ELM suppression

- ergodisation of plasma edge
- harmonic oscillations

### ELM frequency control

- pellet pace making: (convective ELMs?)
- pedestal impurity radiation

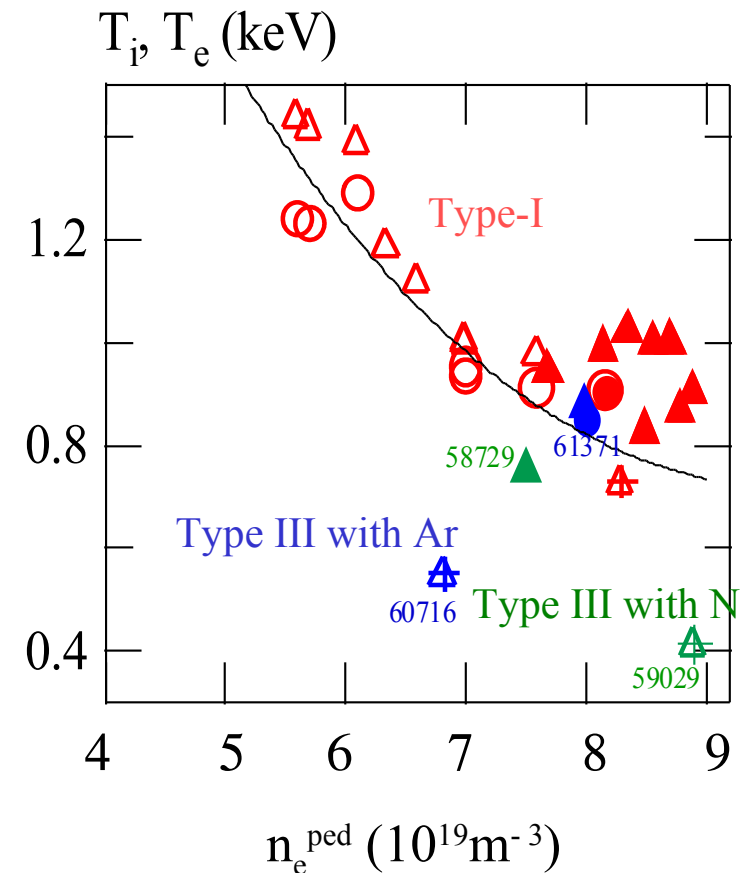
2) degraded confinement

decrease  $\nabla P$  further, and :

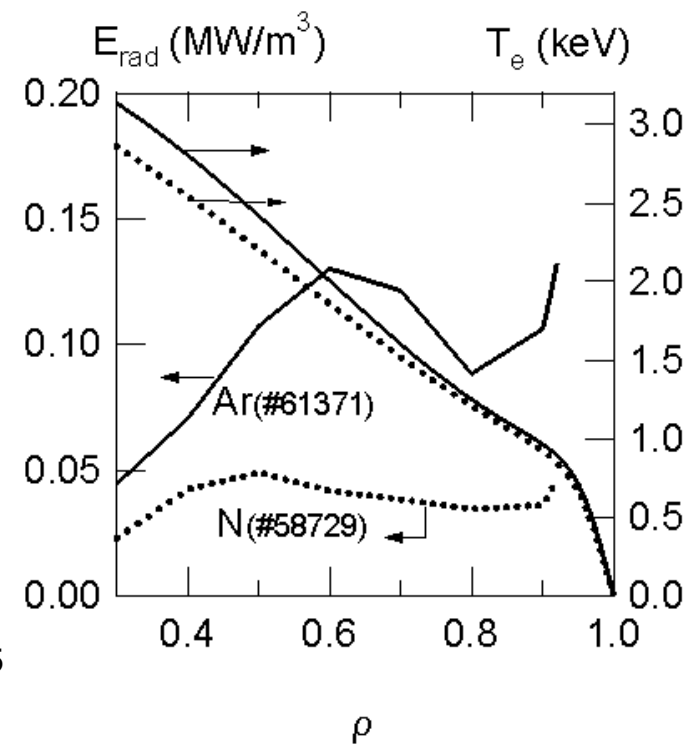
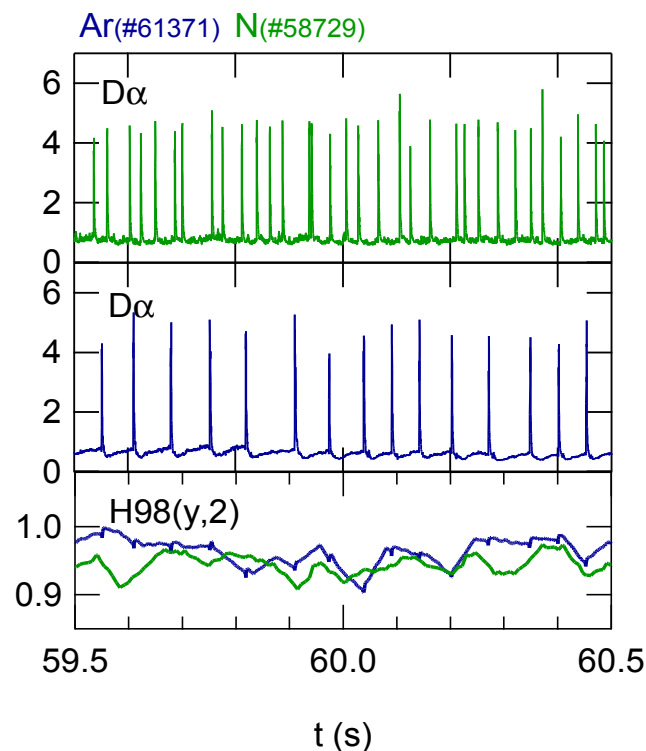
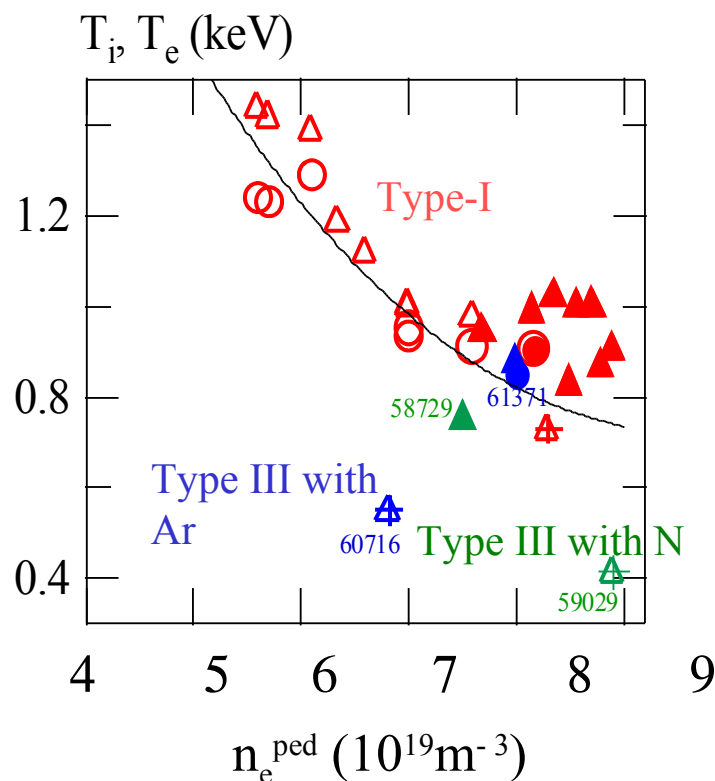
find a scenario with high  $W$  and low  $W_{ped}$

increase  $I_p$  to recover  $W$

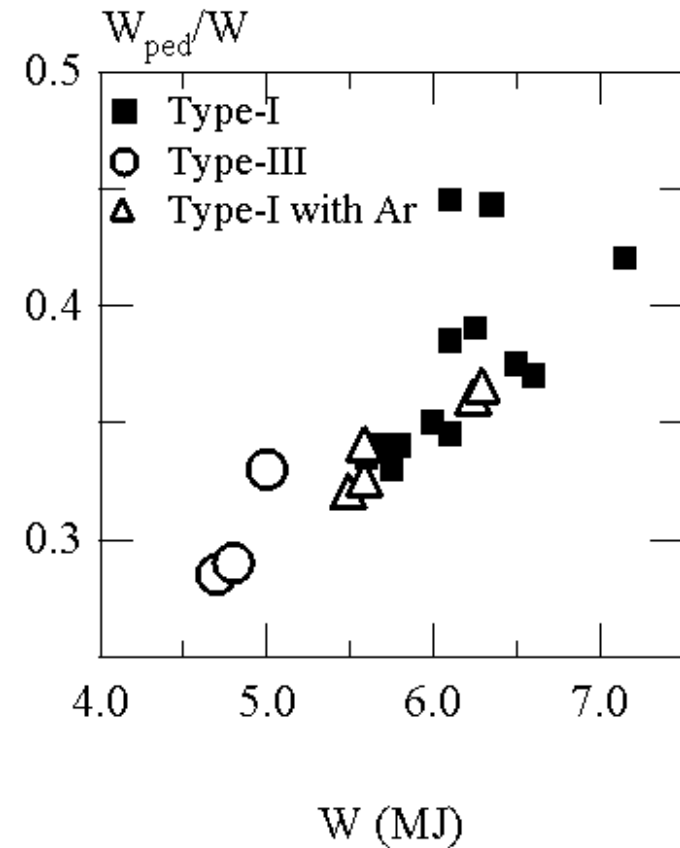
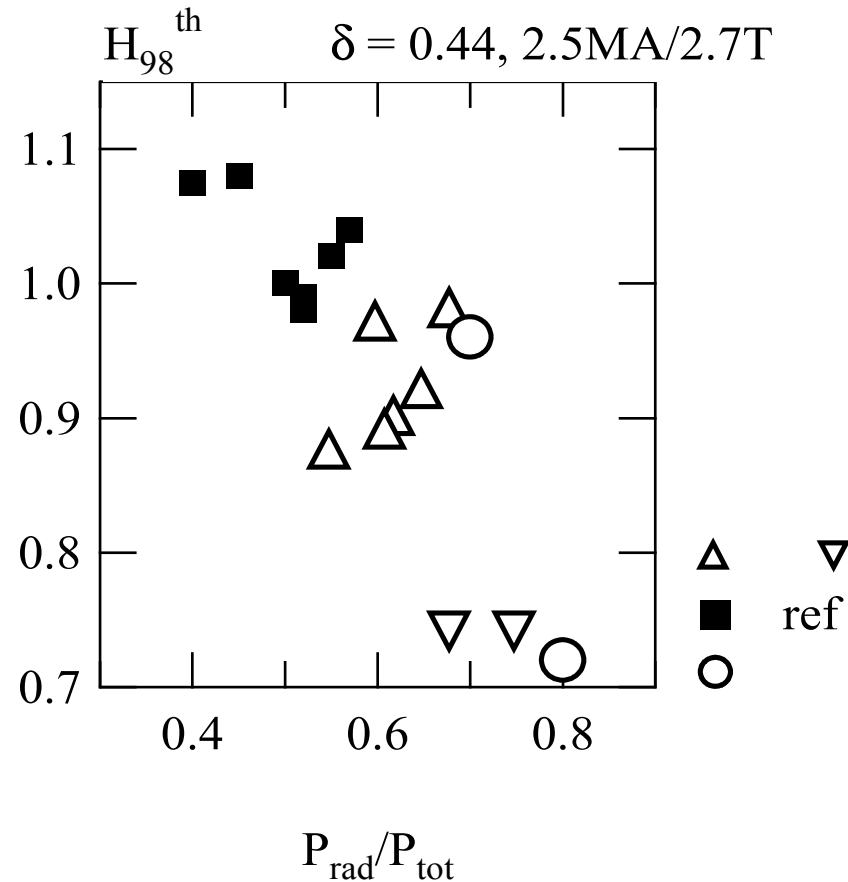
→ scenario with Type III ELMs at high  $I_p$



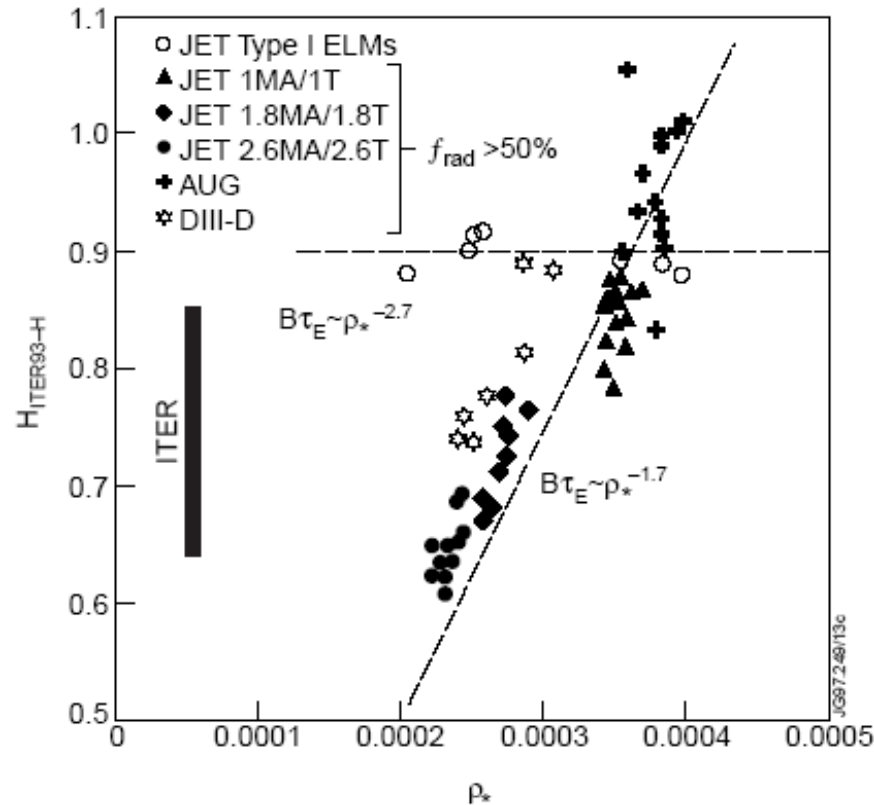
1) confinement ~not affected: control the Type I ELM frequency with pedestal radiation (alternatively, use radiation to maintain  $T_e^{ped}$  just below threshold for Type I ELMs ?)



## Pedestal radiation reduces $W_{ped}$ and total stored energy ( $W$ )



# Degradation / gyro-Bohm ITERH93-P scaling is observed at low $\rho^*$

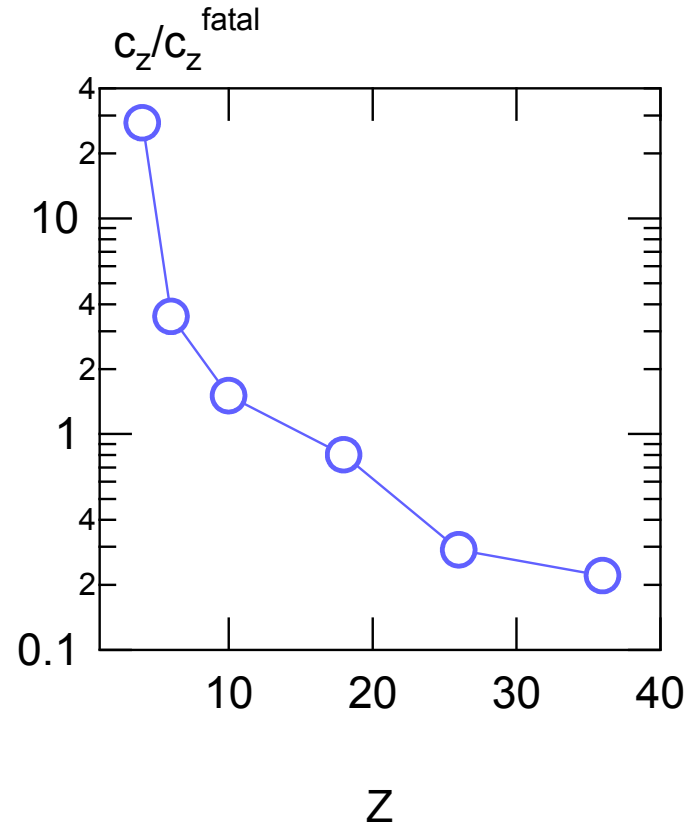
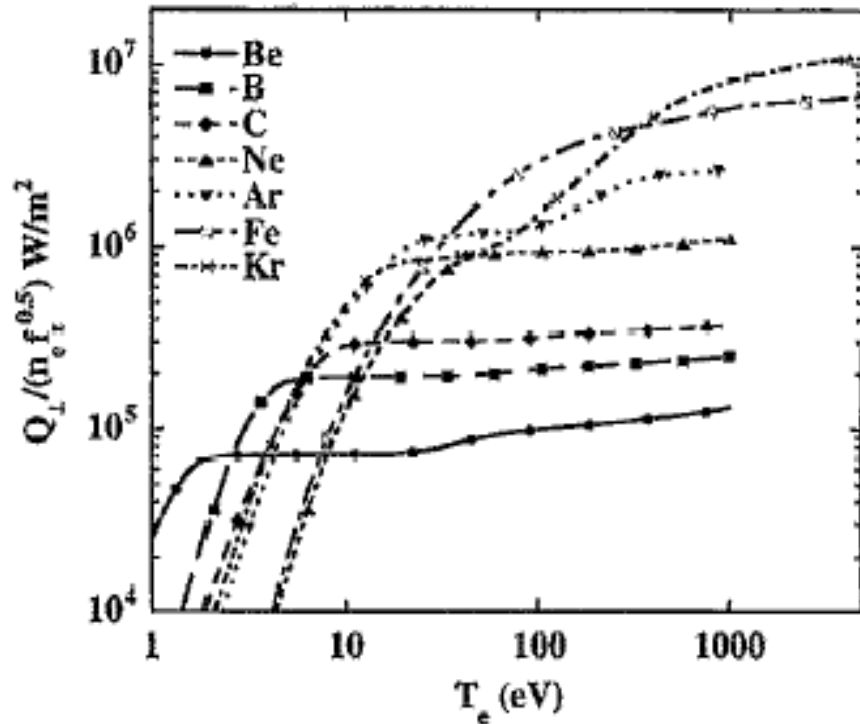


G.F. Matthews et al., NF 39 (1999) 19 - 40.

# Z~Kr minimizes the impurity concentration required to control $W_{ped}$ in ITER

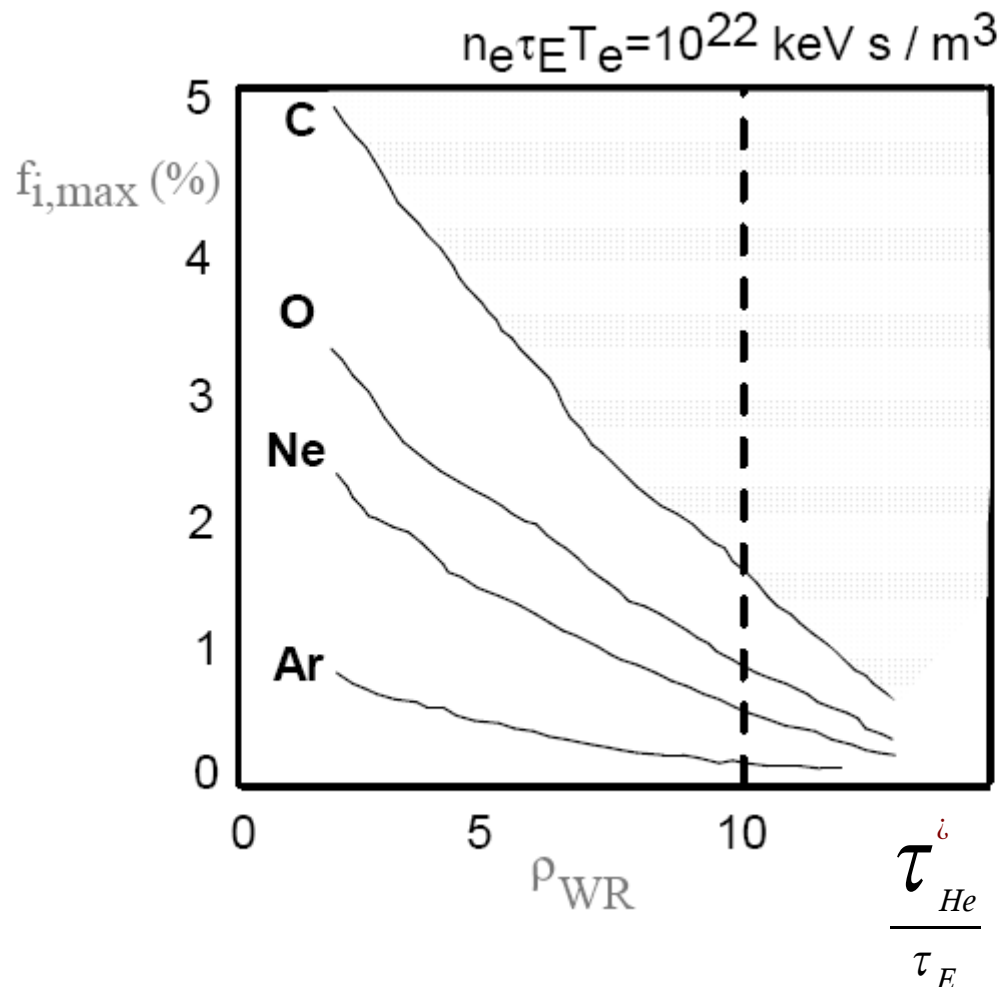
D. Post, et al., Phys. Plasma, 2 (1995) 2328-2336.

$$\begin{cases} Q_i = -\kappa \frac{\partial T_e}{\partial r} \\ \frac{\partial Q_i}{\partial r} = -n_e n_Z L_Z(T_e) \end{cases} \Rightarrow Q_i^2 \approx 2n_e^2 c_z \kappa \int_0^{T_e} L_Z(T_e) dT_e$$



$$\begin{aligned} Q_i &= 0.1 \text{ MW/m}^2 \\ n_e &= 0.8 \times 10^{20} \text{ m}^{-3} \\ \kappa &= 2 \times 10^{20} \text{ m}^{-1} \text{ s}^{-1} \end{aligned}$$

Low edge  $\tau_p$  (as  $\sim$  provided by Type I ELMs) is needed to control impurity accumulation in the core.

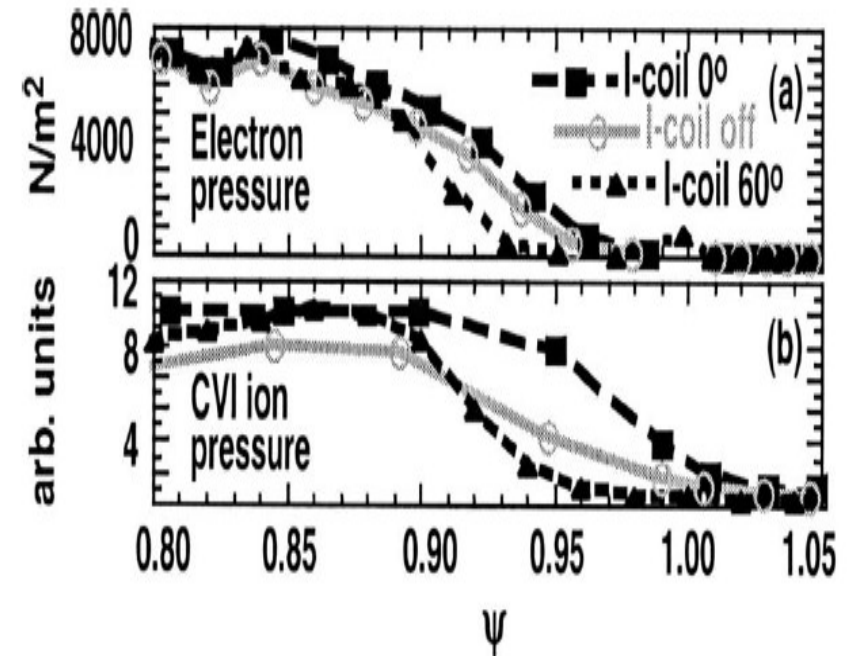
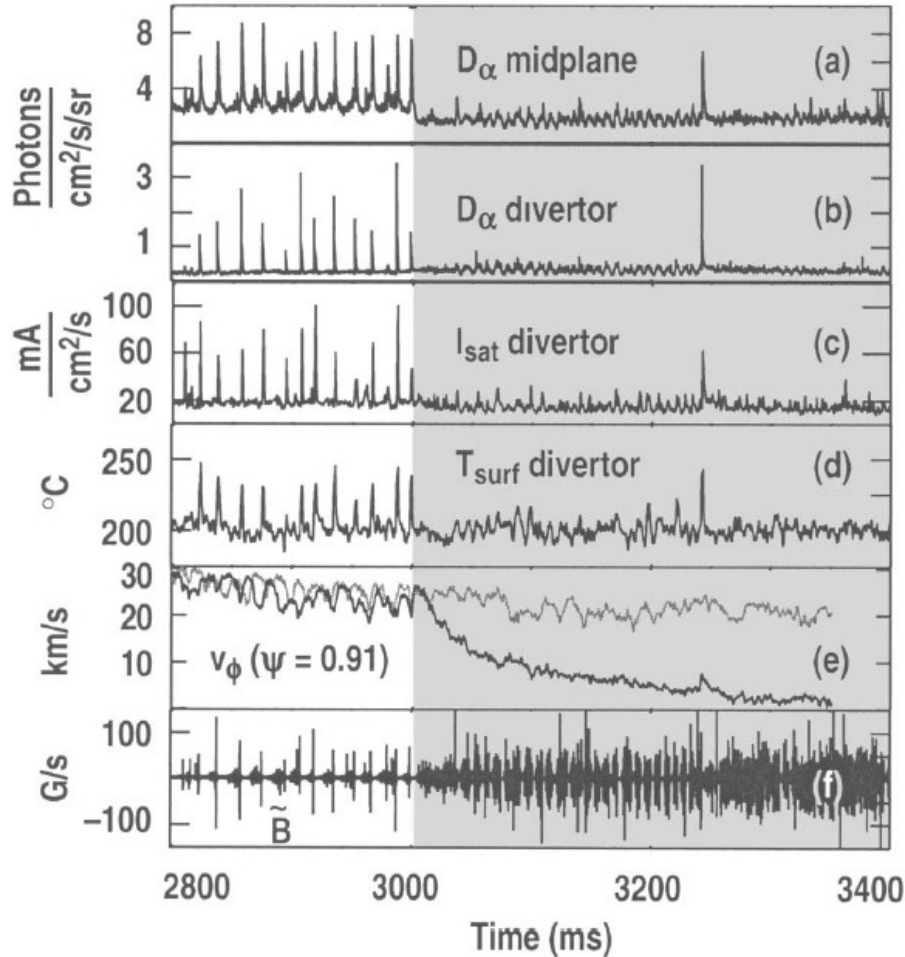


Maximum impurity concentration for steady-state solution depends on  $\tau_{He}^i / \tau_E$

U. Samm et al., JNM 241-243 (1997) 827-832.



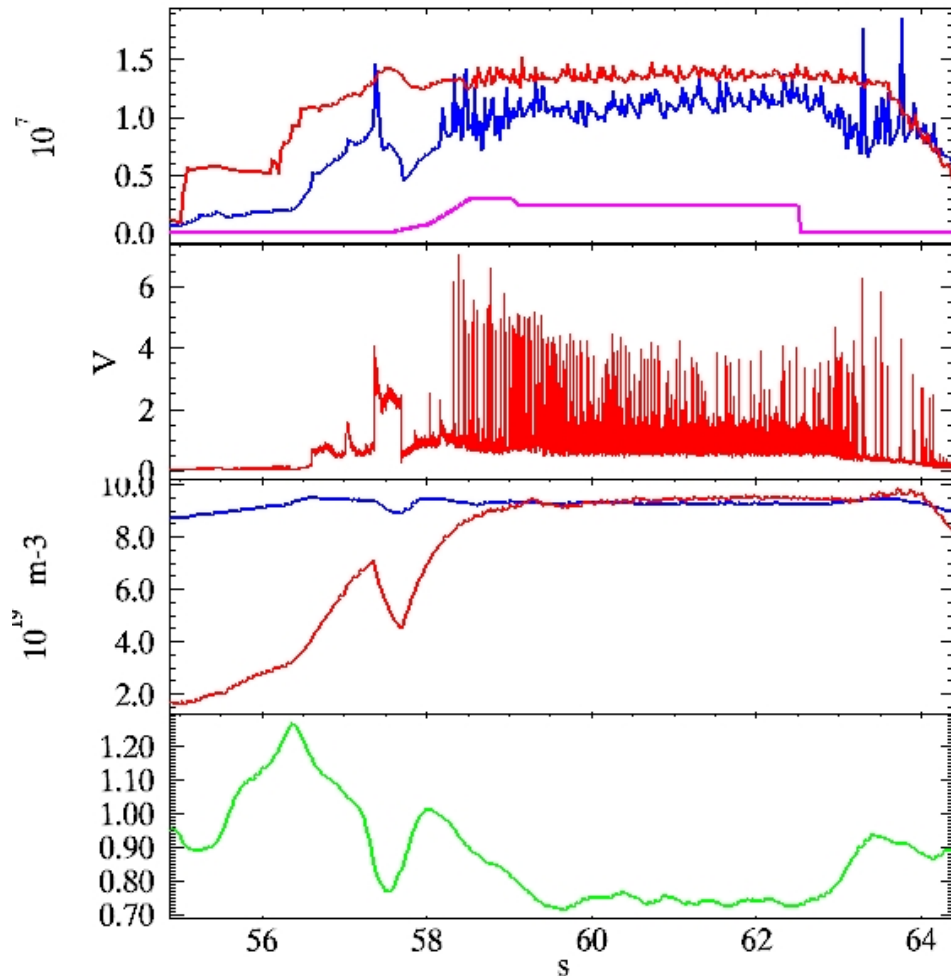
## Pedestal CVI ion pressure increases in ELM suppression experiments with ergodic coils in DIII-D



T. Evans, R. Moyer, P.R. Thomas et al.,  
 Phys. Rev. Lett. **92** (2004) 235003.

## 2) use radiation to produce Type III-ELM regime

HT3 configuration, 2.5MA/2.0T ( $q_{95}=2.6$ ) N seeding



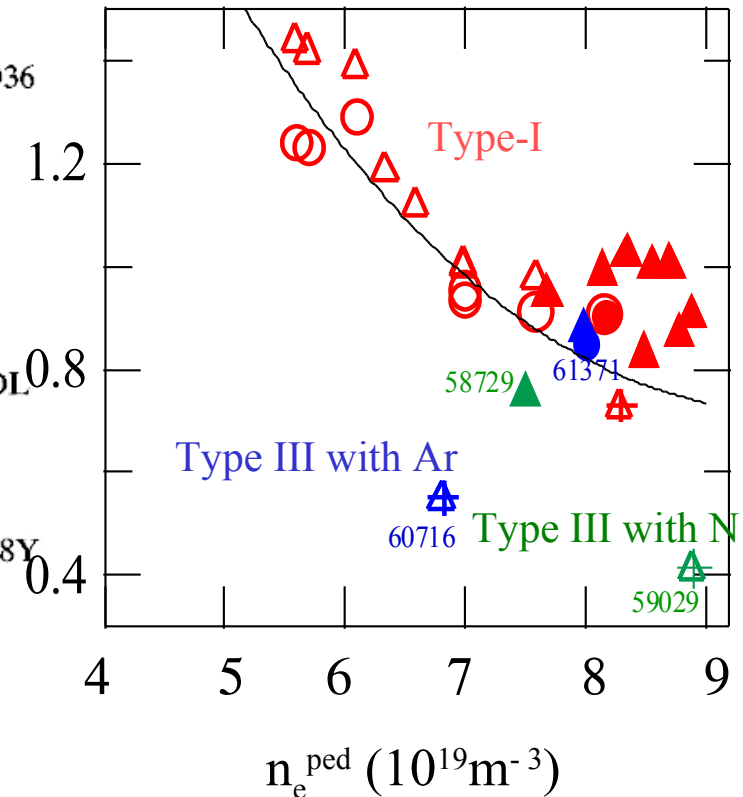
— 59029 MG3/YTO  
Seq=84 (0)  
— 59029 BOL4/TOPI  
Seq=10 (0)  
— PROC/NNORME15

— 59029 DD/S3-AD36

— 59029 NET/AV  
Seq=108 (0)  
— 59029 SCAL/GDL  
Seq=111 (0)

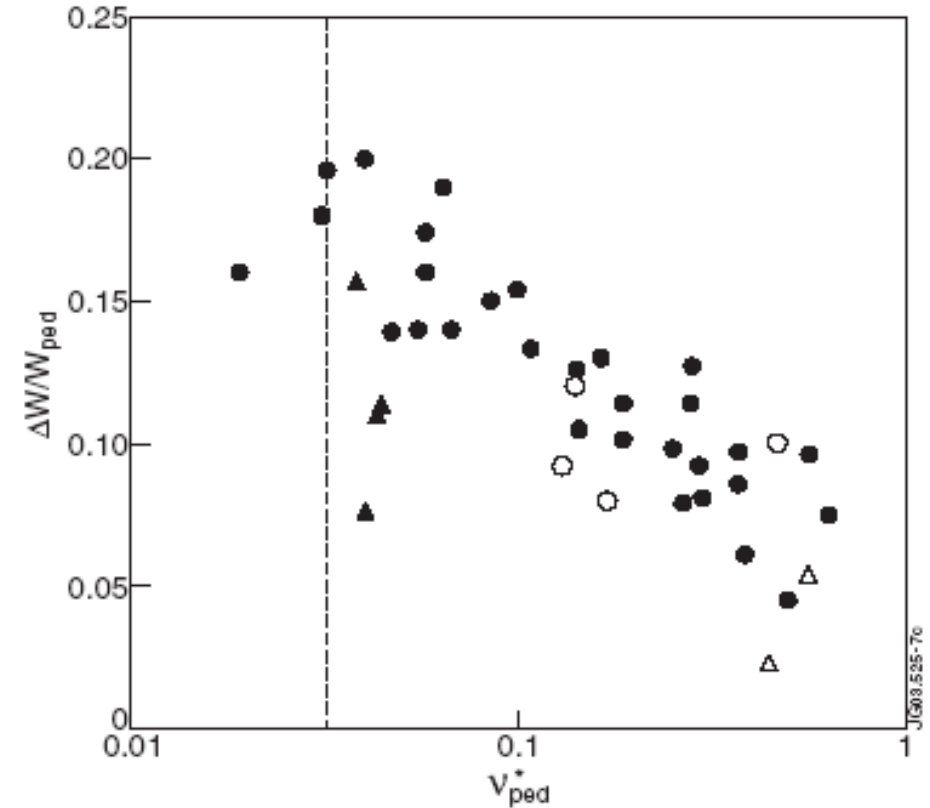
— 59029 SCAL/H98Y  
Seq=111 (0)

$T_i, T_e$  (keV)



## Remaining issues include:

- Type III ELM regime at low  $v$ ?
- Core dilution (will high  $I_p$  help?)
- Is edge  $\tau_p$  low enough?
- In case of hybrid scenario: is type III regime compatible with hybrid scenario?



## Conclusion:

- Impurity radiation may be used as a tool to control  $W_{ped}$
- Additional requirements for integrated scenario include:

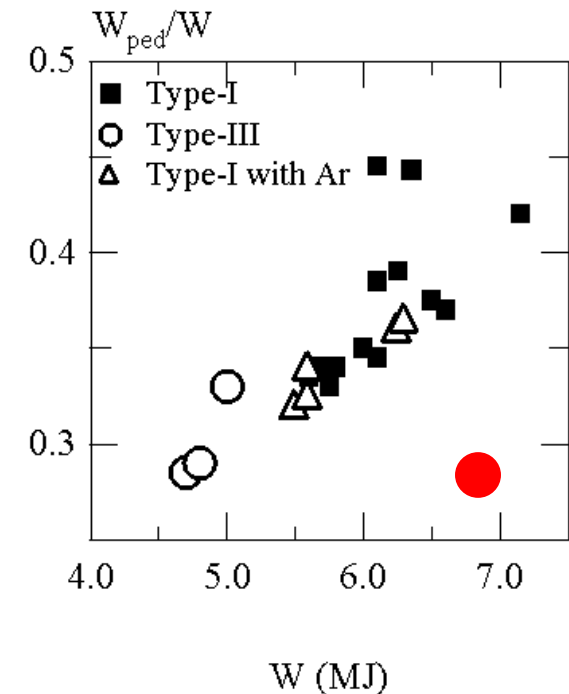
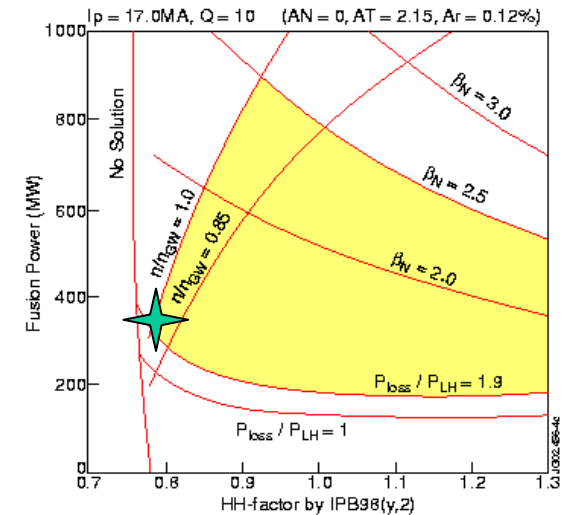
→ maintain low edge  $\tau_p$  for particle removal

→ If  $W_{ped}$  significantly decreased, then need to recover stored energy:

break profile stiffness : how?

Recover  $W$  by other means (experiments planned in 2006 at JET):

Type III H-mode → needs 17MA in ITER  
Hybrid scenario ?



→ use radiation to maintain  $T_e^{\text{ped}}$  just below threshold for Type I ELMs ?

1) Determine what impurity level is required depending on:

choice of impurity species

Local/edge injection

2) consequences on core performances

Dilution

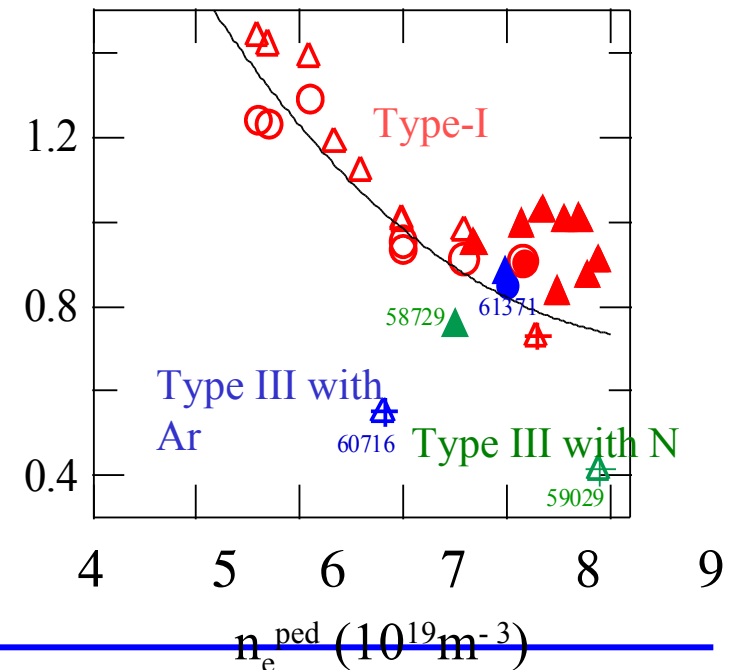
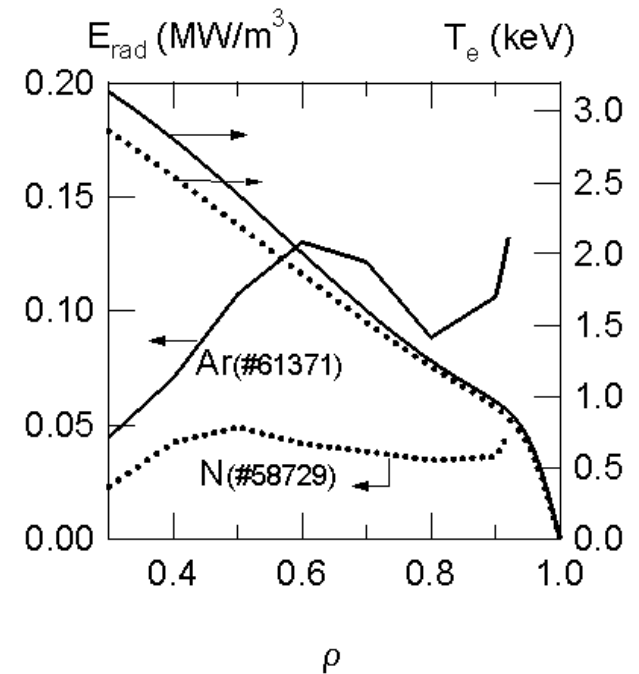
Energy content

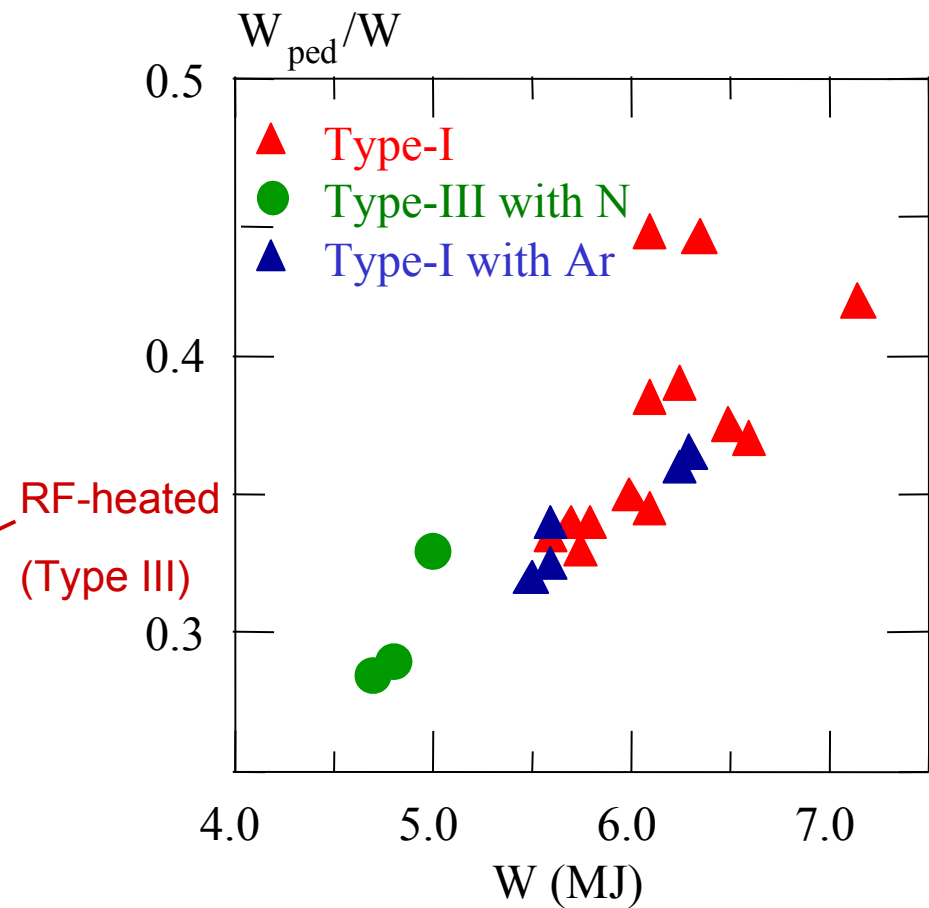
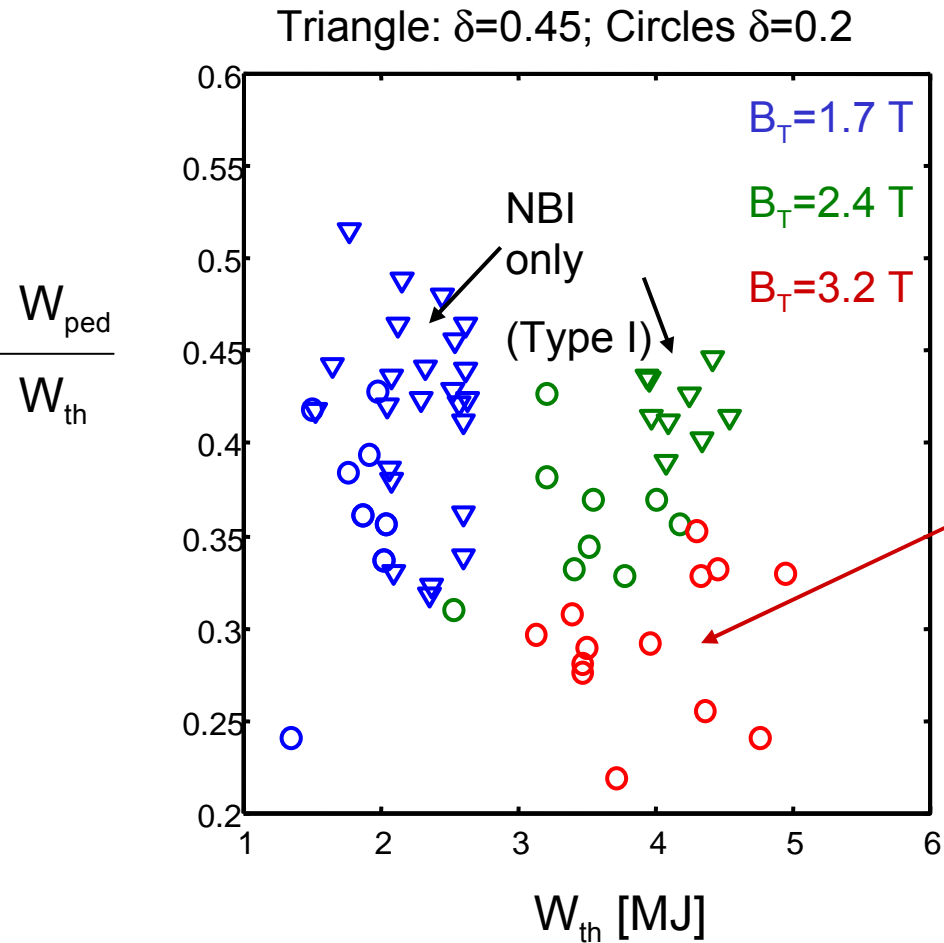
Impurity accumulation:

non steady-state once ELMs are removed

how to get low edge  $\tau_p$ ?

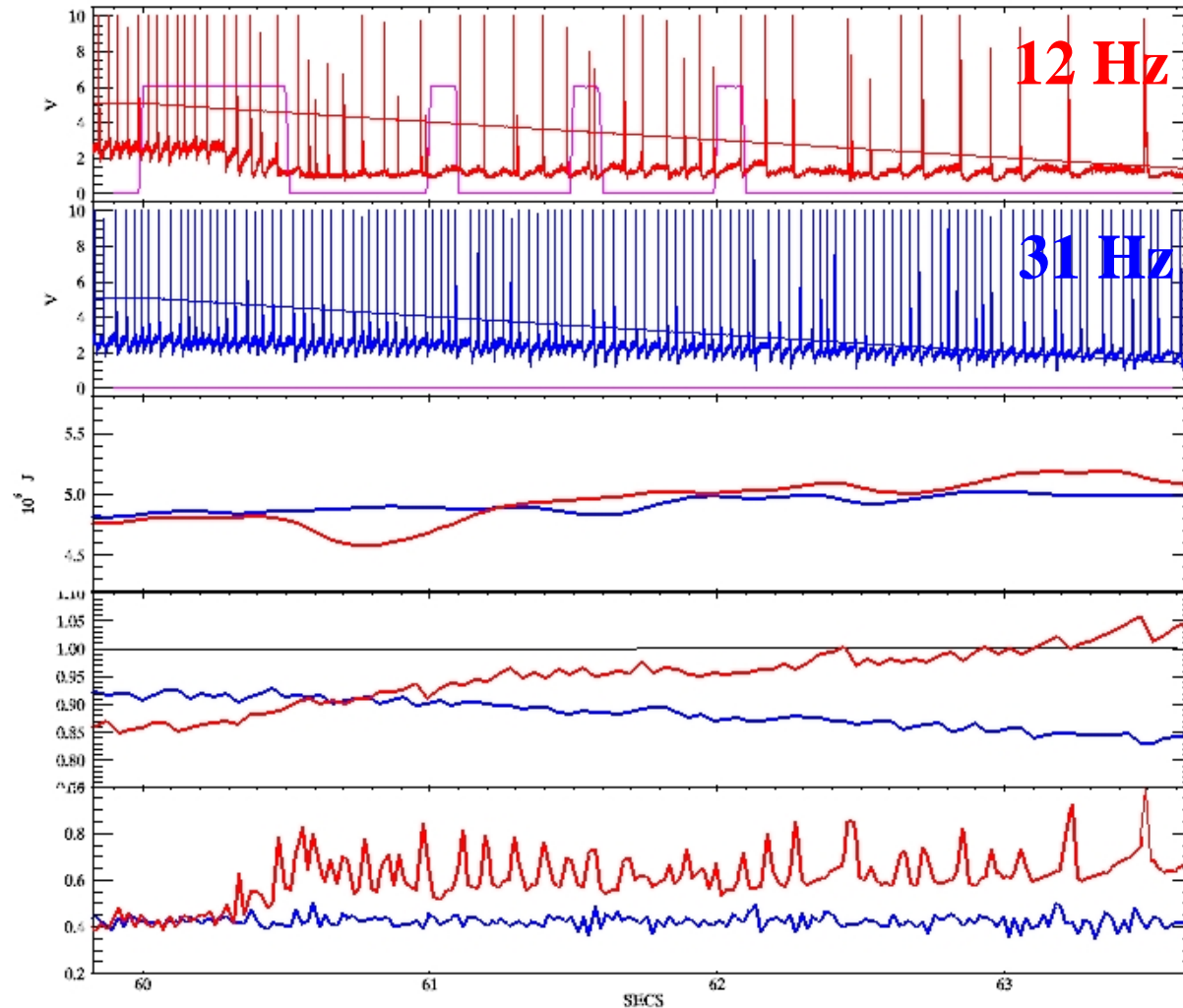
high pumping efficiency required





$f_{\text{ELM}}$  decreases with Ar seeding : - effect of collisionality ( $Z_{\text{eff}} \uparrow$ ) ?  
 - signature of Type I ELMs ( $P_{\text{sep}} \downarrow$ )

#53548 with Ar    #53549 without Ar



- EHT configuration (  $d \gg 0.40$  )  
with septum
- 2.3MA, 2.4T,  $P_{\text{tot}}=16\text{MW}$

same  $W_{\text{dia}}$  despite  
 decreased  $P_{\text{sep}}$ .

$$n_e/n_{\text{Gr}}$$

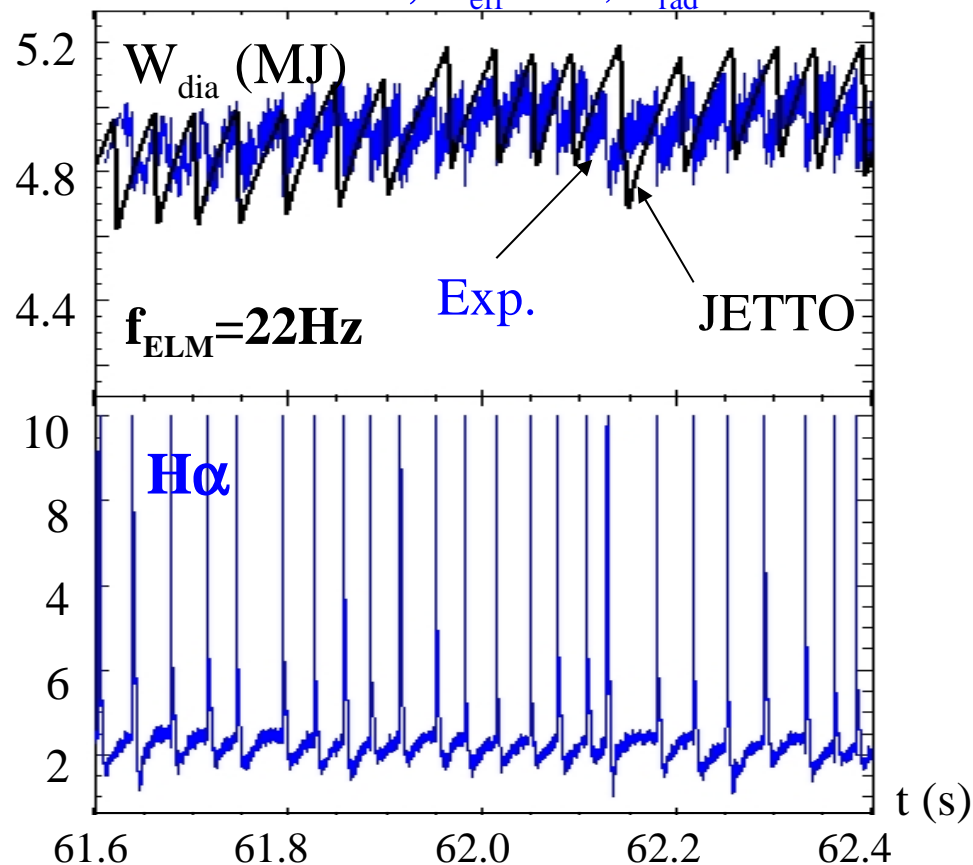
$$P_{\text{rad}}/P_{\text{tot}}$$

## Simple Model for ELMs used in JETTO :

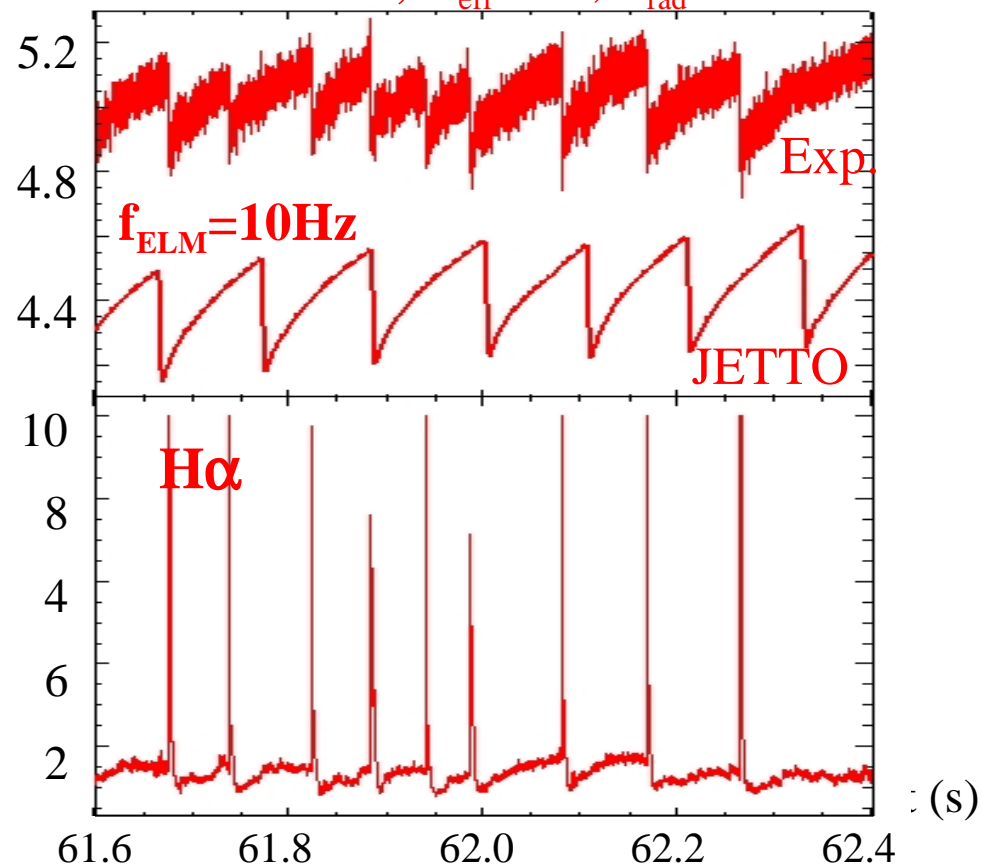
When  $\alpha$  reaches  $\alpha_{\text{crit}}$ , the particle diffusion in the edge is increased.

➔ Exp. decrease of  $f_{\text{ELM}}$  with Ar seeding well reproduced with this model.

#53549 without Ar,  $Z_{\text{eff}}=1.8$ ,  $P_{\text{rad}}^{\text{bulk}}=2\text{MW}$

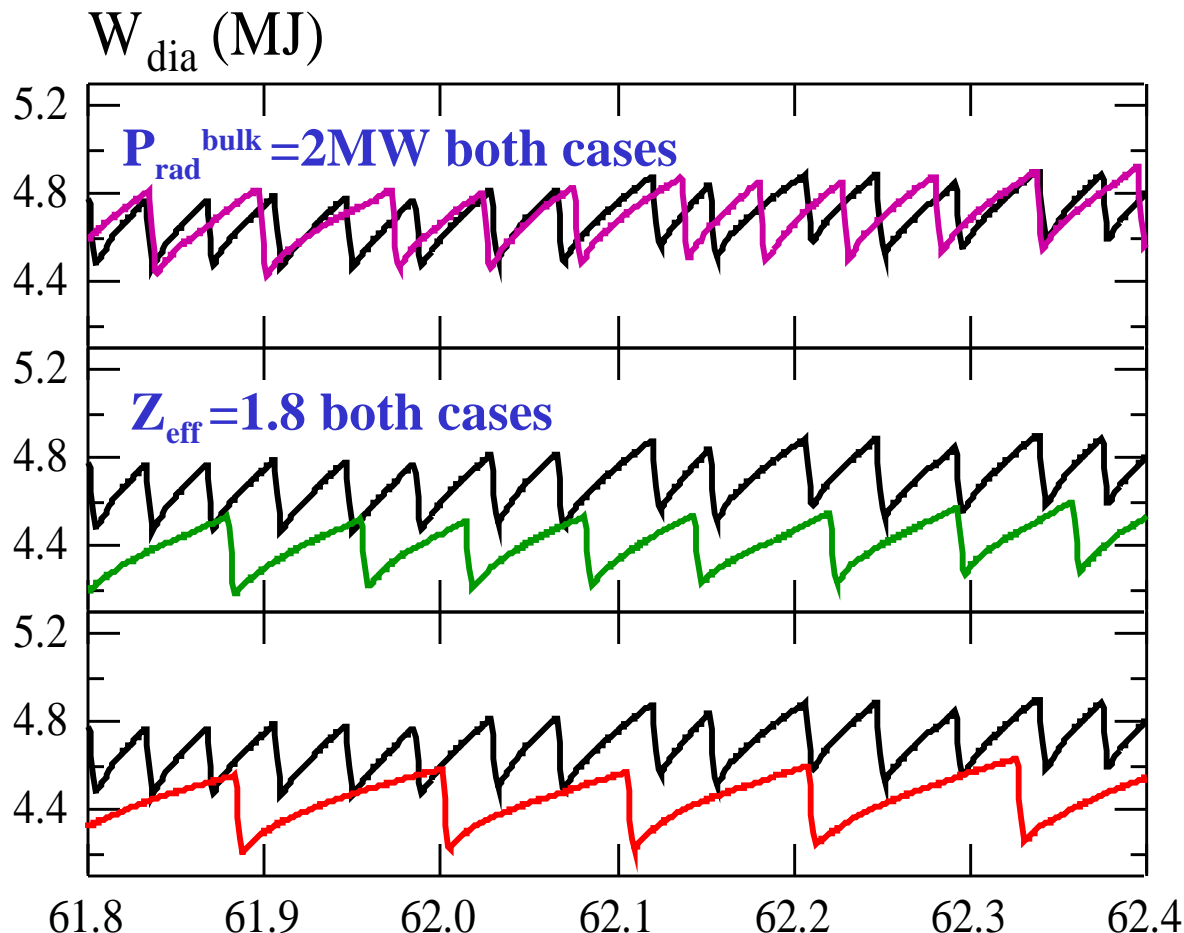


#53548 with Ar,  $Z_{\text{eff}}=2.2$ ,  $P_{\text{rad}}^{\text{bulk}}=6\text{MW}$





The decrease of  $f_{ELM}$  is mainly due to increase of  $P_{rad}^{bulk}$  (weak effect of change in collisionality).



Effect of change in  $Z_{eff}$

$Z_{eff} = 1.8$

$Z_{eff} = 2.2, f_{ELM} \times 0.80$

Effect of change in  $P_{rad}^{bulk}$

$P_{rad}^{bulk} = 2\text{MW}$

$P_{rad}^{bulk} = 6\text{MW}, f_{ELM} \times 0.54$

Combination of both effects

CX and transport effects increase the radiation capability  
 → Decrease  $c/c_{\text{fatal}}$  that is required

