

ETS Numerics – Quality Assessment / Verification

WP09-ITM-IMP3-T2 \implies **WP10-ITM-IMP3-ACT1**

**Maintenance, continuing development,
(verification and validation) of the ETS**

To discuss this week

1. Staffing (find volunteers)

- (a) “Users” – use existing ETS
- (b) “Developers” – extend ETS

2. Verification procedure (see below)

- (a) Basic numerical properties
- (b) Benchmarking vs. existing codes

3. Time span (July? 2010)

Numerical properties

Mandatory

- 1. Approximation**
- 2. Accuracy**
- 3. Convergence**
- 4. Stability**

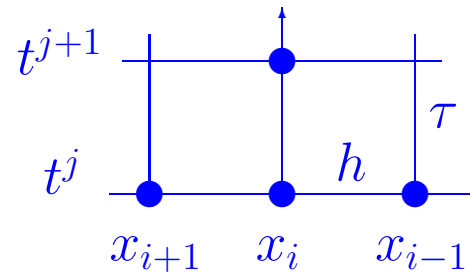
Highly desirable

- 5. Conservation**
- 6. Convection vs diffusion**

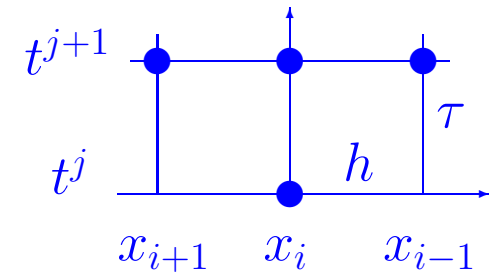
Approximation order (finite differences)

$$\frac{\partial u}{\partial t} = \frac{\partial}{\partial x} \left(D \frac{\partial u}{\partial x} \right) + S$$

FTCS stencil



BTCS stencil



$$\frac{\partial f(x, t)}{\partial t} = \frac{f_i^{j+1} - f_i^j}{\Delta t} + \frac{\partial^2 f}{\partial t^2} \Delta t + \dots \quad \Rightarrow \quad \Delta f = \mathcal{O}(\Delta t), \quad \Delta t = t^{j+1} - t^j = \tau$$

$$\frac{\partial^2 f}{\partial x^2} = \frac{f_{i+1}^j - 2f_i^j + f_{i-1}^j}{\Delta x^2} + \frac{\partial^3 f}{\partial x^3} \Delta x^2 + \dots \quad \Rightarrow \quad \Delta f = \mathcal{O}(\Delta x^2), \quad \Delta x = x_{i+1} - x_i = h$$

The scheme has approximation error of order

$$\Delta f = \mathcal{O}(\Delta t) + \mathcal{O}(\Delta x^2)$$

Caveat: For $\mathcal{N} = t/\Delta t$ time steps the error can accumulate and the **overall error** can be estimated as

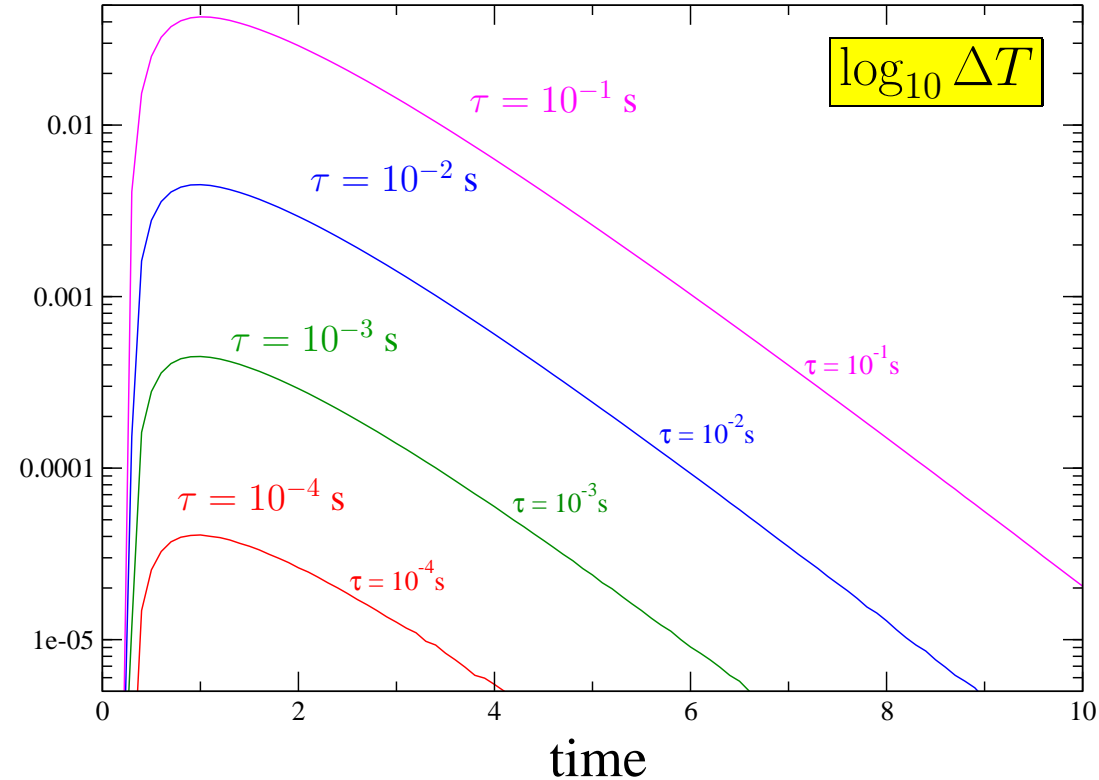
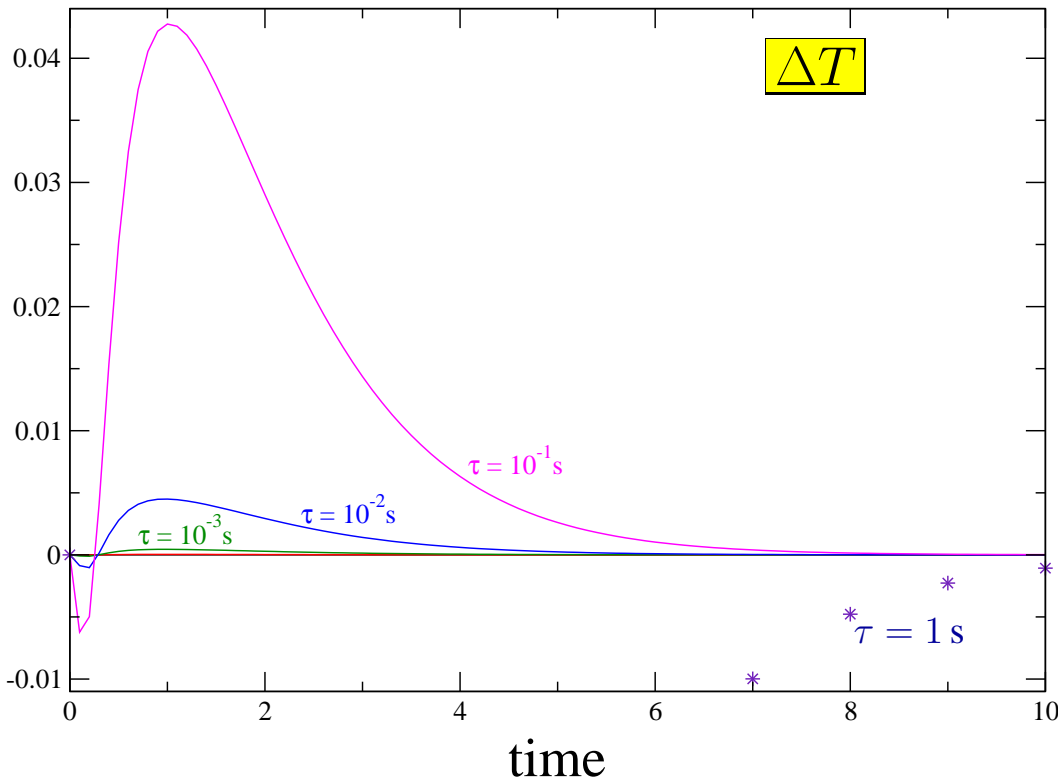
$$\mathcal{N} \times \Delta f = \frac{t}{\Delta t} [\mathcal{O}(\Delta t) + \mathcal{O}(\Delta x^2)] = \mathcal{O}(1)$$

so that no **convergence** occurs.

Numerical accuracy and convergence (examples)

$$\frac{3}{2} (V')^{-5/3} \frac{\partial}{\partial t} \left[(V')^{5/3} nT \right] = \frac{1}{V'} \frac{\partial}{\partial \rho} \left(V' \langle (\nabla \rho)^2 \rangle \chi \frac{\partial T}{\partial \rho} \right) + P$$

Time step dependence



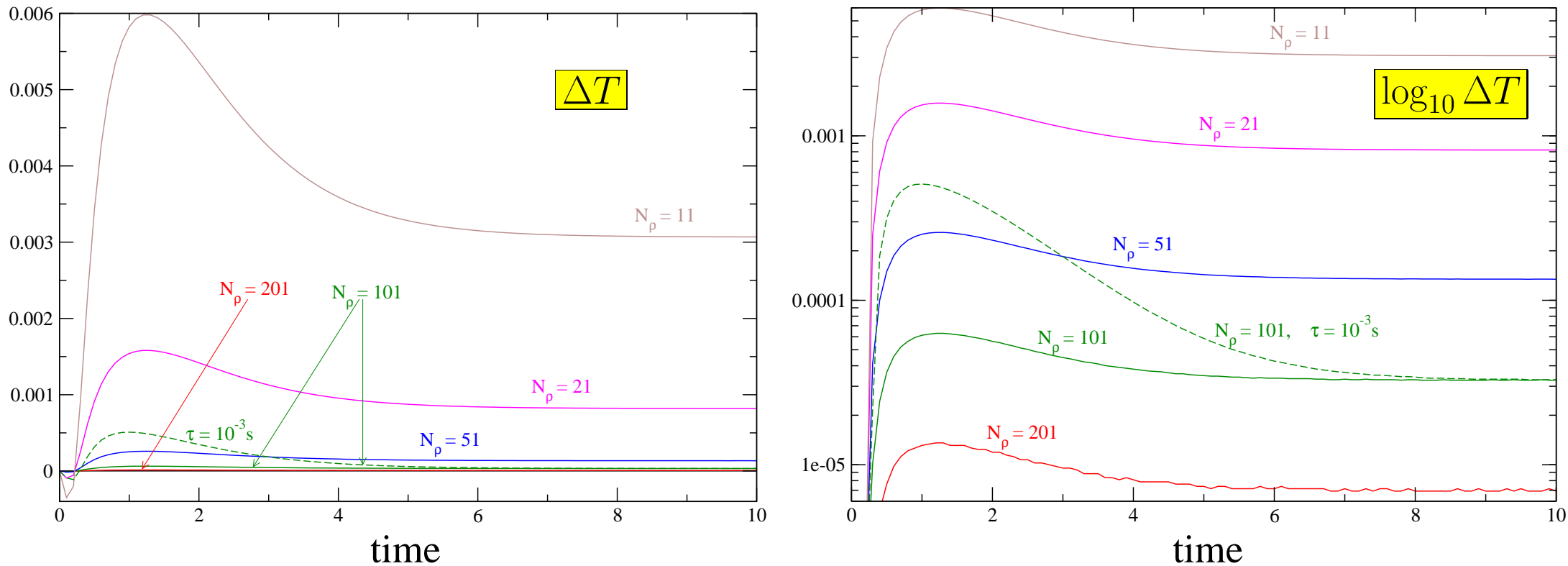
Maximum deviation as function of time for different time steps τ . Reference run $\tau = 10^{-5}$ s.

$$\Delta T = \max_{\rho} (T - T_{ref}),$$

$$T_{ref} = T(\rho, t) \text{ calculated @ } \tau = 10^{-5} \text{ s, } N_{\rho} = 501$$

Numerical accuracy and convergence (cont.)

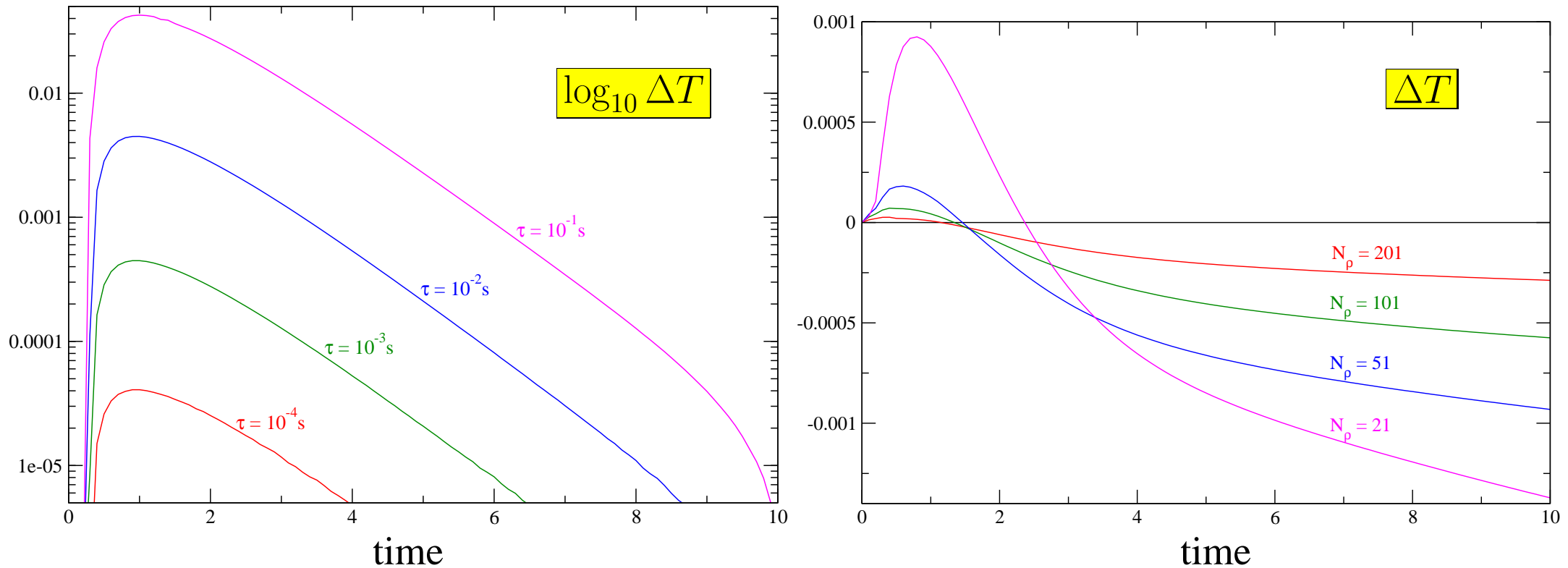
Space step dependence



Maximum deviation as function of time for different grid sizes and $\tau = 10^{-5}$ s (dashed curve $\tau = 10^{-3}$ s).

Numerical accuracy and convergence (cont.)

Equilibrium (EMEQ) included



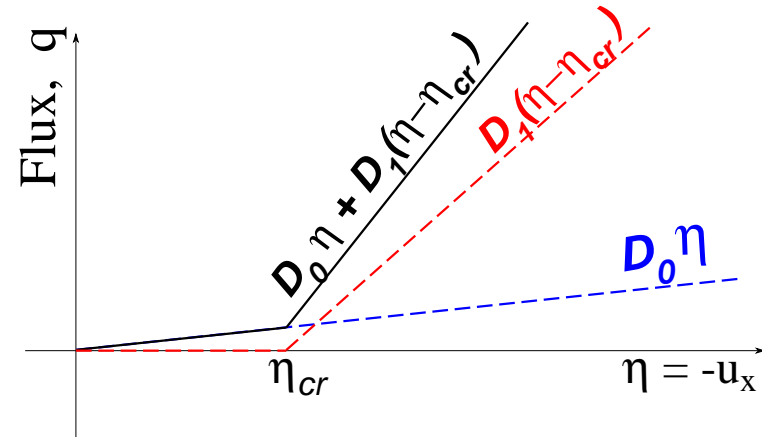
Maximum deviation as function of time for different grid sizes and $\tau = 10^{-5}$ s (dashed curve $\tau = 10^{-3}$ s).

Stability

Stiff diffusion equation

$$\frac{\partial u}{\partial t} = \frac{\partial}{\partial x} \left(D_0 \frac{\partial u}{\partial x} + D_{an} \left(\frac{\partial u}{\partial x} + \eta_{cr} \right) \right) + S$$

$$D_{an} = \begin{cases} D_1 \gg D_0, & \text{if } \left| \frac{\partial u}{\partial x} \right| > \eta_{cr} > 0, \\ 0, & \text{if } \left| \frac{\partial u}{\partial x} \right| < \eta_{cr}, \end{cases}$$



Straightforward approximation

$$\frac{\hat{u}_i - u_i}{\tau} = D_{i+1/2} \frac{\hat{u}_{i+1} - \hat{u}_i}{\Delta x^2} - D_{i-1/2} \frac{\hat{u}_i - \hat{u}_{i-1}}{\Delta x^2} + S_i$$

requires a tiny time step

$$\tau \approx 10^{-5} s \leq 10^{-4} \frac{a^2}{D}.$$

Possible scheme improvement (iterations with $0 \leq \sigma \leq 1$)

$$\frac{\hat{u}_i - u_i}{\tau} = \left(\sigma D_{i+1/2} + (1 - \sigma) \hat{D}_{i+1/2} \right) \frac{\hat{u}_{i+1} - \hat{u}_i}{\Delta x^2} - \left(\sigma D_{i-1/2} + (1 - \sigma) \hat{D}_{i-1/2} \right) \frac{\hat{u}_i - \hat{u}_{i-1}}{\Delta x^2} + S_i$$

Conservation

Exact conservation law: $u_t = (Du_x)_x + S \Rightarrow \frac{\partial}{\partial t} \int_0^a u dV + \Gamma = \int_0^a S dV$

$$\frac{\hat{u}_i - u_i}{\tau} = D_{i+1/2} \frac{\hat{u}_{i+1} - \hat{u}_i}{\Delta x^2} - D_{i-1/2} \frac{\hat{u}_i - \hat{u}_{i-1}}{\Delta x^2} + S_i \quad 0 \leq i \leq N$$

$$\begin{aligned}
 \frac{\hat{u}_0 - u_0}{\tau} &= D_{1/2} \frac{\hat{u}_1 - \hat{u}_0}{\Delta x^2} + S_0 & i = 0 \\
 \frac{\hat{u}_1 - u_1}{\tau} &= D_{3/2} \frac{\hat{u}_2 - \hat{u}_1}{\Delta x^2} - D_{1/2} \frac{\hat{u}_1 - \hat{u}_0}{\Delta x^2} + S_1 & i = 1 \\
 + \\
 \frac{\hat{u}_2 - u_2}{\tau} &= D_{5/2} \frac{\hat{u}_3 - \hat{u}_2}{\Delta x^2} - D_{3/2} \frac{\hat{u}_2 - \hat{u}_1}{\Delta x^2} + S_2 & i = 2 \\
 \dots & \dots & \dots \\
 \frac{\hat{u}_N - u_N}{\tau} &= D_{N+1/2} \frac{\hat{u}_{N+1} - \hat{u}_N}{\Delta x^2} - D_{N-1/2} \frac{\hat{u}_N - \hat{u}_{N-1}}{\Delta x^2} + S_N & i = N
 \end{aligned}$$

Numerical conservation law is exact for grid function

$$\Delta x \sum_{i=0}^N \frac{\hat{u}_i - u_i}{\tau} = D_{N+1/2} \frac{\hat{u}_{N+1} - \hat{u}_N}{\Delta x} + \Delta x \sum_{i=0}^N S_i \Rightarrow \Gamma = -D_{N+1/2} \frac{\hat{u}_{N+1} - \hat{u}_N}{\Delta x}, \quad S = \Delta x \sum_{i=0}^N S_i$$

Conservation (cont.)

Integral conservation law:
$$\frac{\partial}{\partial t} \int_0^a u dV + \Gamma|_a = \int_0^a S dV$$

Numerical conservation law:
$$\Delta x \sum_{i=0}^N \frac{\hat{u}_i - u_i}{\tau} = D_{N+1/2} \frac{\hat{u}_{N+1} - \hat{u}_N}{\Delta x} + \Delta x \sum_{i=0}^N S_i$$

- **Both conservation laws are exact.**
- **Existence of a numerical conservation ensures that some basic physics constraints are fulfilled.**
- **Convergence does not ensure that \implies Conservation is highly desirable**

However, a form of numerical conservation law should be conforming with a numerical scheme.

- \implies Change of numerics implies a change of the conservation law.
- \implies Not every numerical approximation possess a conservation property.
- \implies Non-conserving methods should not be used in ETS.
- \implies Conservation is not a consequence of approximation because the total error can be large enough.
- \implies Cross-process conservation laws have to be included.

Examples of significance:

- Electron-ion equipartition
- Particle conservation for impurities
- Volt-second consumption

Convective terms

$$\frac{\partial u}{\partial t} = \frac{\partial}{\partial x} \left(D \frac{\partial u}{\partial x} - V u \right) + S$$

The first-order upwind scheme

$$\frac{\hat{u}_i - u_i}{\tau} = D_{i+1/2} \frac{\hat{u}_{i+1} - \hat{u}_i}{\Delta x^2} - D_{i-1/2} \frac{\hat{u}_i - \hat{u}_{i-1}}{\Delta x^2} - \min(V_{i+1/2}, 0) \frac{u_{i+1} - u_i}{\Delta x} - \max(V_{i-1/2}, 0) \frac{u_i - u_{i-1}}{\Delta x} + S_i$$

$= 0, \text{ if } V_{i+1/2} > 0 \qquad = 0, \text{ if } V_{i-1/2} < 0$

is stable but non-conservative.

The simple scheme

$$\frac{\hat{u}_i - u_i}{\tau} = D_{i+1/2} \frac{\hat{u}_{i+1} - \hat{u}_i}{\Delta x^2} - D_{i-1/2} \frac{\hat{u}_i - \hat{u}_{i-1}}{\Delta x^2} - \frac{V_{i+1/2} u_{i+1/2} - V_{i-1/2} u_{i-1/2}}{\Delta x} + S_i$$

is conservative but can become unstable.

In transport modelling convection is usually small.

⇒ Problems can arise if $V \geq D/a$

V&V proposals for IMP3

Users

1. Perform accuracy tests for each ETS solver.
 - (a) Simple cases (including non-smooth, non-continuous coefficients).
 - (b) Manufactured solutions.
 - (c) Select the reference time and space steps $\{\Delta t, \Delta x\}$ for further studies.
2. Perform series of runs on conservation property.
3. Convection vs. diffusion.
4. Benchmarking: Run the test cases with ASTRA, JETTO, CRONOS.
5. Documentation for pp. 1 – 4 by July 2010.

⇒ Validation procedure.

Developers

1. Extend existing solver to include stiff transport.
2. Add more solvers (CRONOS, finite elements, ...)

start_time_loop

READ_INPUT

start_iteration_loop

EQUILIBRIUM

→ **Internal iterations: Exit if** ($\max \Delta_E < 10^{-5}$)

SOURCE

TRANSPORT

CONVERGENCE_CHECK

→ $\max \Delta_I < 10^{-4}$?

end_iteration_loop

CONVERGENCE_CHECK

→ $\max \Delta_T < 10^{-3}$?

TIME_ADVANCE $t=t+\Delta t, \dots$

end_time_loop

- Optimize the procedure
- Automated time step