

Application of the parameterized EPED1 model to time-dependent transport simulation

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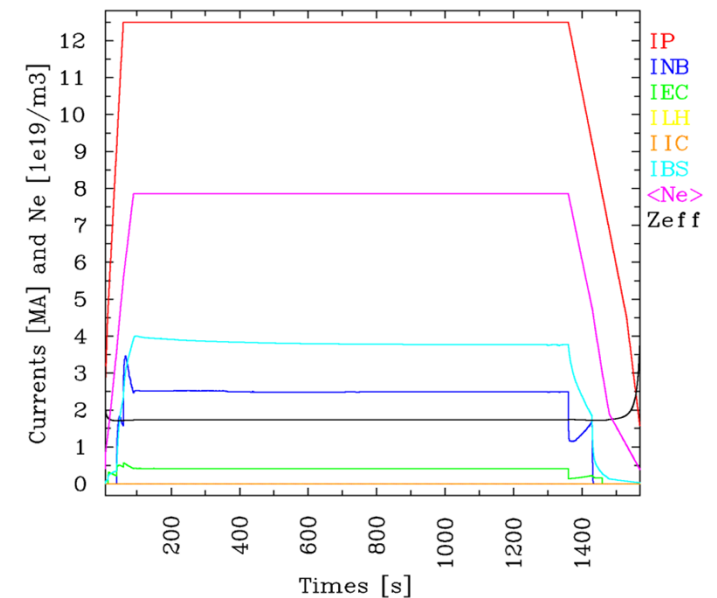
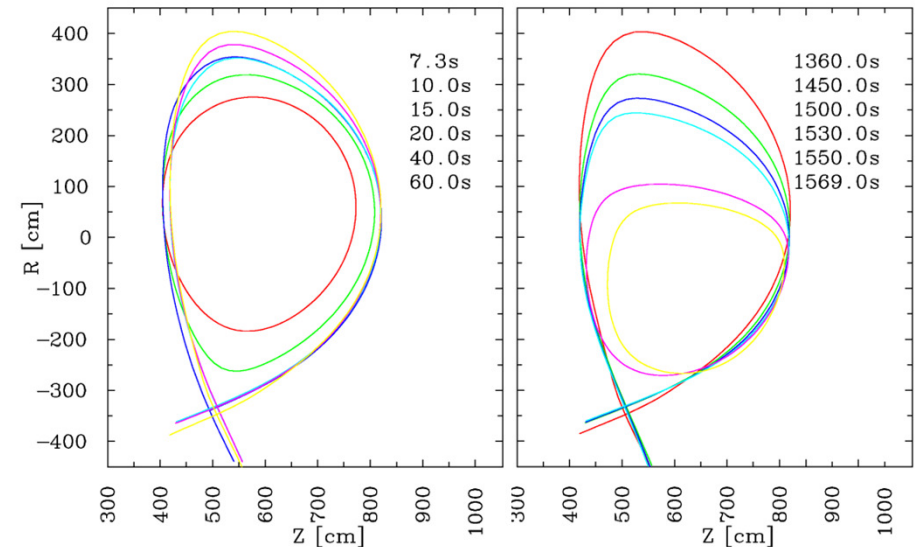
**Acknowledgement : LLNL, IO/Monaco
ISM(EU) and P. Snyder (GA) – EPED1 results**

ITER hybrid mode with a parabolic density shape

- 12.5MA scenario, large bore startup
- 1300s of current flat-top & $n_{GW} \sim 9.9e19 \text{ m}^{-3}$
- $n_e(0, \text{flat-top}) = 8.5e19 \text{ m}^{-3}$ & parabolic shape
- Coppi-Tang transport model
- $T_e(\text{ped}) \sim 3\text{-}4\text{keV}$, $\rho_{\text{tor}}(\text{ped}) \sim 0.95$
- Effective sawteeth when $q_{\text{min}} < 0.97$
- Be and Ar impurities, self-consistently with $Z_{\text{eff}}(t) = 1.7 + 2.3 * (n_{e0}(t_0)/n_{e0}(t))^{2.6}$ (V. Lukash)
- 33MW of NB (off-axis) & 20MW of EC (2 co-ELs and 1 UL-LSM)
- 60s ramp-up (XPF at about 15s and L-H transition at 40s)
- 210s ramp-down (H-L transition 70s after EOF)

At $t=1359\text{s}$ ($t_{\text{EOF}} = 1360\text{s}$)

- $Q \sim 9.6$ & $P_\alpha \sim 101\text{MW}$ \rightarrow high Q (>5.0) with $P_{\text{aux}} = 53\text{MW}$
- $H_{98} \sim 1.24$ & $I_i(3) \sim 0.75$ \rightarrow improved confinement
- $\beta_N \sim 2.5$ & $\beta_p \sim 0.82$ \rightarrow high betas
- $I_{\text{BS}} \sim 3.8\text{MA}$, $I_{\text{NB}} \sim 2.5\text{MA}$ & $I_{\text{EC}} \sim 0.4\text{MA}$ $\rightarrow f_{\text{NI}} \sim 0.54$



Parameterized EPED1 model

- ❑ EPED1 results on ITER H-mode and hybrid mode scenarios are provided by P. Snyder (ISM working session in JET Nov. 2011)
- ❑ 9 inputs : (I_p , $n_{e,ped}$, Z_{eff} , β_N , R , a , κ , δ , B_t)
- ❑ 4 outputs : (Δ_{ped} , P_{ped} , Δ_{top} , P_{top})

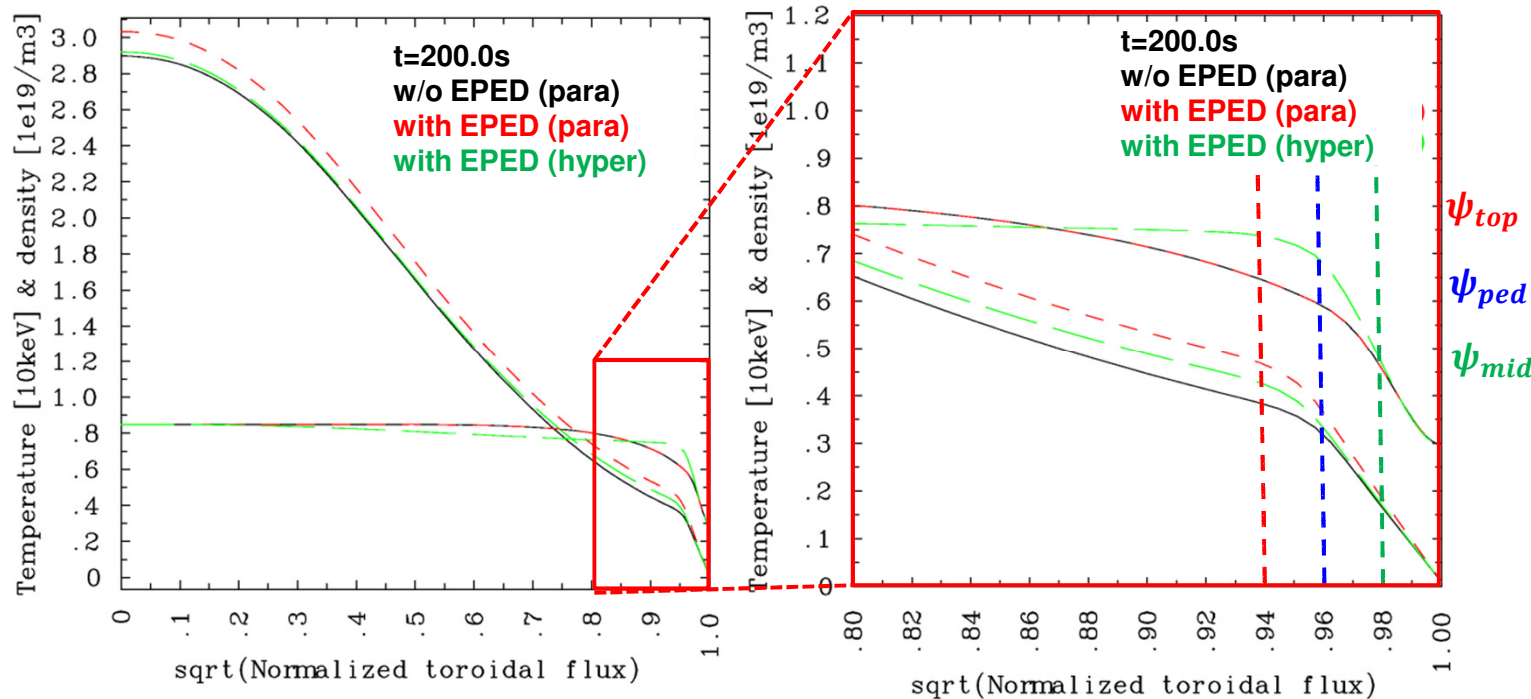
- ❑ When the density profile is prescribed in time-dependent transport simulations, the input $n_{e,ped}$ need to be determined either
 - ❑ assuming a constant value, $n_{e,ped} = r_1 * n_{e,0}$, then allowing the prescribed density profile to vary.
 - ❑ or using iterations, $n_{e,ped} = n_e(\Delta_{ped}^{(k+1)}) = EPED1 \{ n_e(\Delta_{ped}^{(k)}), \dots \}$, with a fixed density profile

- ❑ The pedestal height ($T_{e,top}$, not $T_{e,ped}$) can be feedback controlled
 - ✓ using X_e & X_i to satisfy $n_{e,top} * T_{e,top} + n_{i,top} * T_{i,top} = P_{top}(1 - \Delta_{top})$

Hyperbolic pedestal density profile

- ❑ A hyperbolic tangent shape pedestal density profile [PPCF46, P. Snyder] is **modified** to have only **4 control parameters** for entire density profile (also for density peaking).
- ❑ 2 exponents (α, β) and 2 density ratios at the pedestal and edge (r_1, r_2).

$$n_e(\psi) = n_{e0} \left\{ (1 - r_2) \left(c_1 \left[H \left(1 - \frac{\psi}{\psi_{ped}} \right) \left(1 - \left(\frac{\psi}{\psi_{ped}} \right)^\alpha \right)^\beta \right] + c_2 \left[\tanh \left(2 \frac{1 - \psi_{mid}}{1 - \psi_{ped}} \right) - \tanh \left(2 \frac{\psi - \psi_{mid}}{1 - \psi_{ped}} \right) \right] \right) + r_2 \right\}$$



$$\alpha = \beta = 1.0$$

$$r_1 = 0.80$$

$$r_2 = 0.35$$

$$n_e(0) = n_{e0}$$

$$n_e(\psi_{ped}) = r_1 n_{e0}$$

$$n_e(1) = r_2 n_{e0}$$

$$c_2 = \left(\frac{r_1 - r_2}{1 - r_2} \right) \frac{1}{2 \tanh(1)}$$

$$c_1 \cong 1 - c_2 (1 + \tanh(1))$$

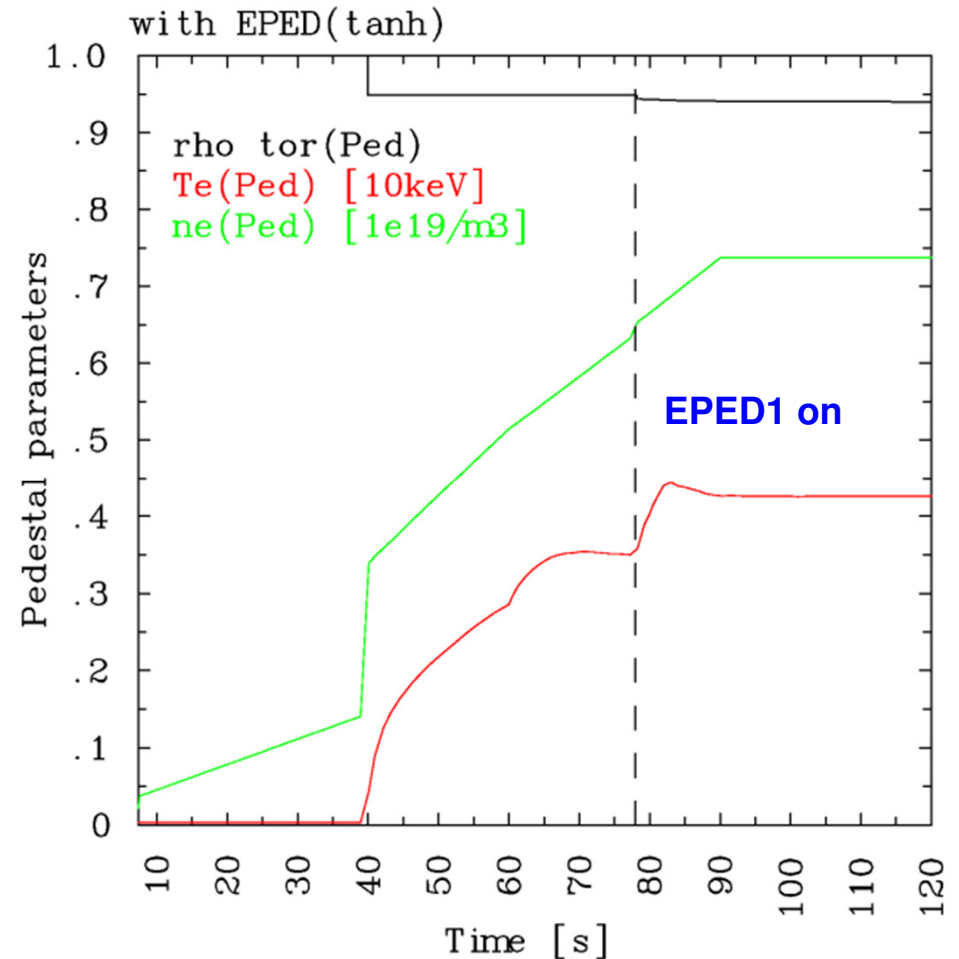
Application to CORISCA simulation

❑ Multi-dimensional linear interpolation / extrapolation

- ✓ up to 9 input dimensions
- ✓ extrapolation up to several tens %
- ✓ switched on only when it can work properly.
- ✓ Indexing for fast 1 dimensional calculation (2^m instead of $n_1 * n_2 * \dots * n_m$)

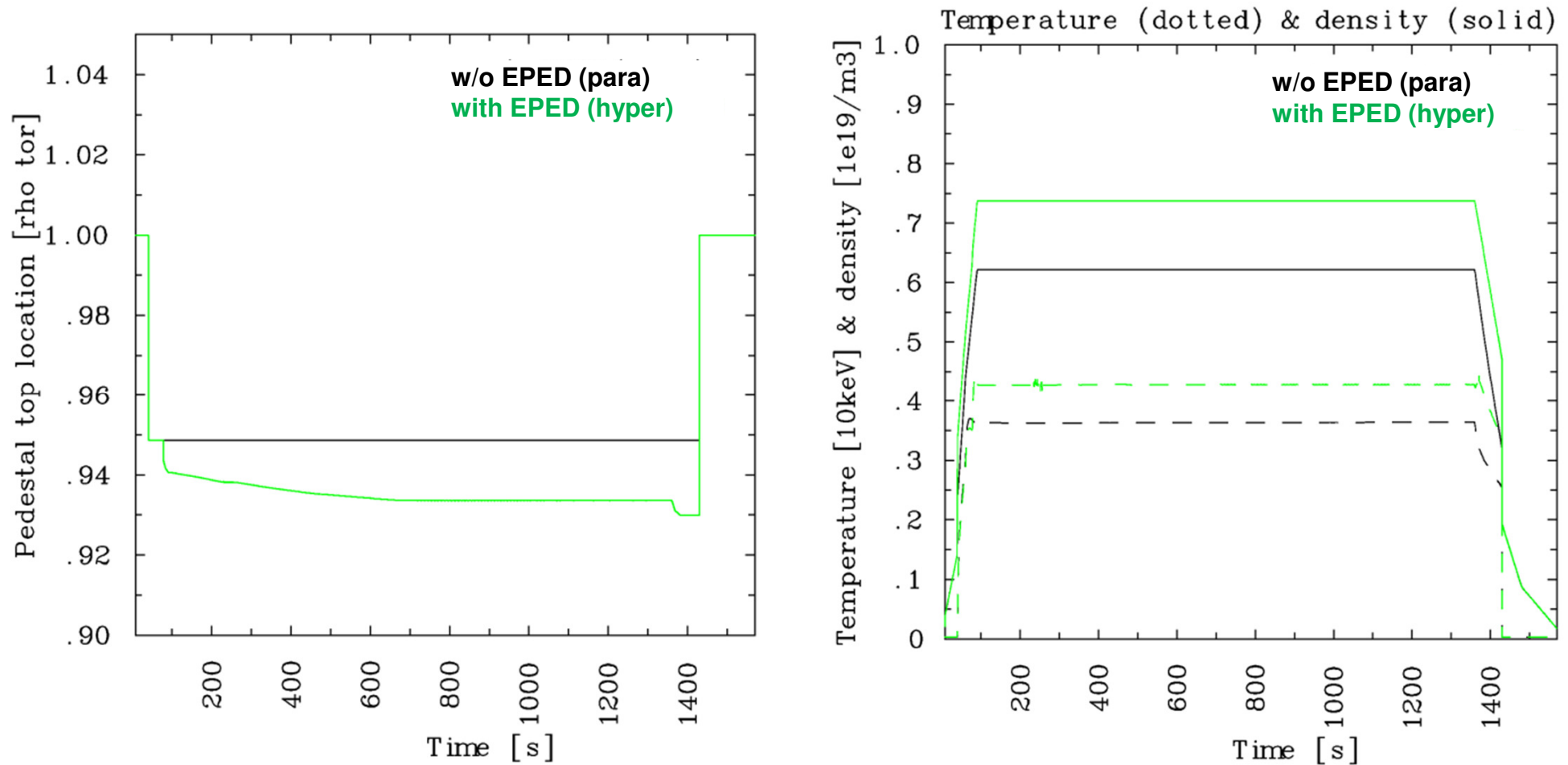
❑ Feedback control

- ✓ $X_{e,i}(\rho > 1 - \Delta_{top}, t^{k+1})$
 $= f_{mult} * X_{e,i}(\rho > 1 - \Delta_{top}, t^k)$
- ✓ f_{mult} is determined by measuring P_{top} / P_{top}^{EPED}



Evolution of the pedestal width & height

- The EPED1 pedestal width & height are larger & higher than previously used settings.

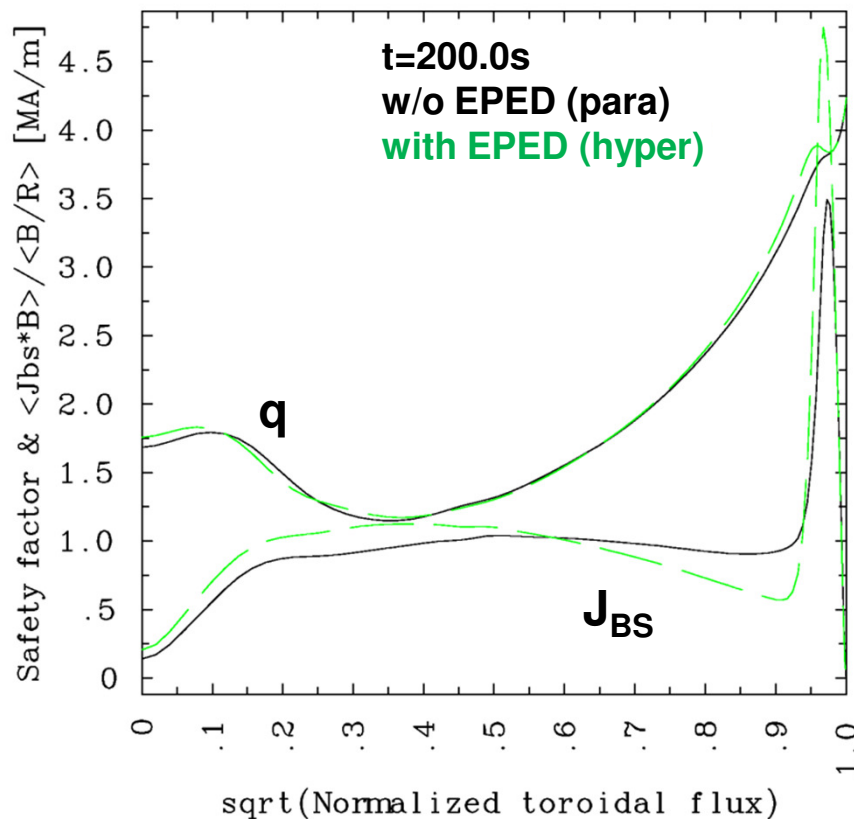


Bootstrap current density profile

- Total bootstrap currents are similar, although their profile shapes are different

For the same n_{e0} ($= 8.5e19 / m^3$)

- w/o EPED (para) : IBS = 3.759 MA



- with EPED (hyper) : IBS = 3.776 MA

