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# On Core-SOL Integration in Scenario Modelling for ITER

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Presented at the ISM meeting,  
Cadarache, March 8, 2011

# Core-SOL integration: why?

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**ISM goal:** find a scenario providing necessary performance, consistent with available controls and satisfying technical limitations on all systems involved

**SOL/Divertor:** one of such systems with limitations on target power loading, He removal and plasma detachment, controlling core fuelling and impurity contamination

*Over-simplified SOL models offer little help:*

could provide separatrix  $n$  and  $T$ , **but**  
no neutrals, no geometry, no wall interactions

→ *no relation to technical limitations,*  
*no model of control actuators*

such as gas puff, pumping speed or impurity injection

**No experiment yet** in the parameter range of ITER

→ **Internal consistence** of the model extremely important

# Core-SOL integration: how?

Scenario studies: long time scale (hundreds sec)

SOL/Divertor: time scale of tens msec → quasi-steady-state

→ Direct coupling impractical:

SOL/Div much slower computationally

Indirect (“mediated”) coupling:

parameterization of SOL/Div results

in terms of separatrix parameters

input: power and charged particle fluxes from core

(BC for SOL/Div)

output:  $n_j$ ,  $T_e$ ,  $T_j$ ,  $\Gamma_n$ ,  $E_n$

(BC for core)

Produces solutions for the core consistent with SOL/Div

Translates SOL/Div constraints to the core

Avoids using non-controllable BC (e.g.  $n_{sep}$ ) for the core

*Being used now for operational window studies*

# Episode 7: integration with core

Different time scales for core and edge → direct coupling impractical

Scalings to parameterise SOLPS results → b.c. for ASTRA (1D)

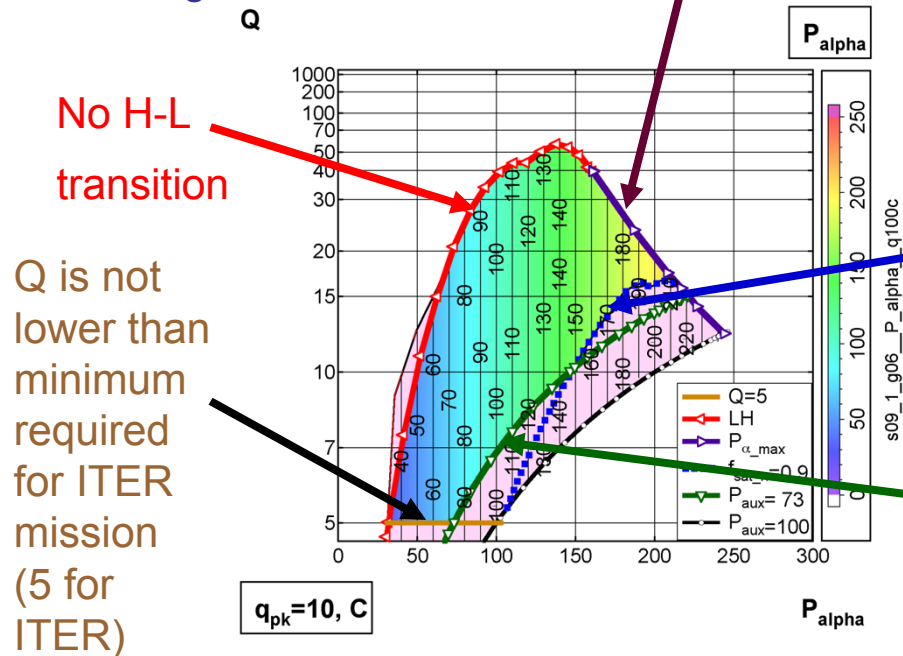
ASTRA: pedestal model;  $(n, T, \Gamma_n, E_n) = F(q_{\perp}, \Gamma_i)$  at separatrix

Control:  $P_{aux}, \Gamma_{core}$  for core;  $\Gamma_{puff}$  for  $q_{pk}, S_p$  for He → real controls

→ Operational window for the whole ITER consistent with divertor

## Window limits

Low-n, high-T, high fusion cross-section branch: no  $P_{\alpha}$  rollover



Throughput within limit, no full detachment

$$f_{sat\_n} = \mu^{0.43} < 0.9$$

Required heating power within design limits (73MW)

## Effect of $q_{pk}$ limitation

